Ausgold delivers 1.28 Moz Maiden Ore Reserve at Katanning

Highlights:

Prefeasibility Study (PFS) ***confirms a 1.28 million ounce Maiden Ore Reserve*** *at the Katanning Gold Project and highlights it as one of the largest undeveloped free-milling open cut gold projects in Western Australia, with low capital costs and substantial scope to increase the total scale of this project in the near term.*

A high 1.47 g/t Au head grade in the initial 6 years of production delivers per year on average 126 koz of gold, generating A$555M of after tax free cashflow to the project over that 6-year period. This cashflow enables an early payback of the A$225M pre-production capital requirements over 1.7 years and sets up a post-tax IRR of 40.7%

Ausgold is focused on becoming Australia's next mid-tier gold producer.

Key Operation Findings:

- *Average annual gold production of 105,000 oz for 11 years using simple open cut mining methods*
- *Maiden Probable Ore Reserve of 32Mt @ 1.25 g/t gold for 1.28 Moz*[1]
- *Project Mineral Resources 56Mt @ 1.21 g/t gold for 2.16Moz*
- *Ore to be processed on-site via conventional gravity and CIL processing facility with a name plate capacity of 3Mtpa,*
- *Demonstrates excellent metallurgical characteristics with gold recoveries over 90%*
- *Project 100% owned*
- *Tier 1 jurisdiction with great access to infrastructure*
- *Connection to power grid with potential to access off-grid wind based renewable*

Key financial forecasts for the PFS

- *LOM revenue of A$2.67 billion*
- *LOM project EBITDA A$981 million*
- *Pre-production capital requirement of A$225 million includes pre-production operating costs*
- *LOM undiscounted post-tax free cashflow, of $540 million (net of pre-production capital costs)*
- *Post-tax* NPV_5 *of A$364M*
- *Internal Rate of Return (IRR) of 40.7% post-tax*
- *All-In-Sustaining Cost (AISC) A$1,370/oz* ***first six years of production***
- *Payback period of 1.7 years*

Environmental and Social considerations

- *Project on existing mining licenses over freehold land where minimal clearing is required*
- *Great access to future infrastructure developments with proximity to a supportive community*
- *Local job creation and economic diversity*
- *Will unlock a new mining province in the Great Southern Region of Western Australia*

[1] *The Company's Maiden Probable Ore Reserve does not include Inferred Mineral Resource*

Highlights (Cont.):

Outstanding Growth potential

- *The Company sees this PFS as the start of a much larger multi-million ounce mining operation supported by multiple exploration opportunities*
- *Larger project has been identified within current Resource using the PFS economics with lower cut-off (>0.4g/t Au) grades this will be the focus of subsequent mining studies*
- *Project designed to be easily expanded to accommodate further exploration success with significant drilling program ongoing targeting further Resource expansion and growth.*
- *Since the May 2022 Resource Estimate, a further 5,000m of RC and 600m diamond drilling has been completed within the Central and Southern zones with a significant number of assays pending that are expected to support further Resource upgrades*
- *Drilling also underway targeting high-grade mineralisation to expand potential underground Resource*

Ausgold Limited (ASX: AUC) (**Ausgold**, or the **Company**) is pleased to announce the results of the Prefeasibility Study (PFS) and Maiden Ore Reserve for the Company's 100%-owned flagship Katanning Gold Project (**KGP** or the **Project**) located 275km south-east of Perth, Western Australia.

Table 1 Key LOM Financial and Physical metrics

Key Metrics	
Life of Mine	11 years after 1.5 years construction
Ore Tonnes Mined	32 Mt
Ore Processing Rate	3 Mt/a
Stripping Ratio	9
Average gold grade – years 1 - 6	1.47 g/t Au
Average gold production (recovered) – years 1 - 6	126 koz
Average gold grade – LOM	1.25 g/t Au
Average gold production (recovered) – LOM	105 koz
Recovered Gold	**1.16 Moz**
Financial Metrics	
Revenue	A$2,669M
All in Sustaining Costs (AISC) – first 6 years production	A$1,370 per oz
All in Sustaining Costs (AISC) – LOM	A$1,481 per oz
Net free cashflow (pre-tax)	A$746M
Net free cashflow (post-tax)	A$540M
EBITDA – Life of Mine	A$981M
Payback period (post-tax)	1.7 years
NPV (pre-tax)	A$515M
NPV (post – tax)	A$364M
Internal Rate of Return (IRR) pre-tax	50.5%
Internal Rate of Return (IRR) post-tax	40.7%
Gold Price Assumption	A$2,300 per ounce
Capital Expenditure and Closure Costs	
Pre-Production Capital and Operating Costs	A$225M
Sustaining Capital Costs	A$31M
Closure Costs	A$8M

Table 2 Mineral Resources and Ore Reserve Inventory

Mineral Resource	Tonnes (Mt)	Grade (g/t Au)	Contained Ounces (Moz)
Measured	19.0	1.31	800,000
Indicated	26.8	1.14	984,000
Inferred	9.5	1.03	370,000
Total	**56.0**	**1.21**	**2,160,000**
Ore Reserve	**Tonnes (Mt)**	**Grade (g/t Au)**	**Contained Ounces (Moz)**
Probable	32	1.25	1,280,000
Total	**32**	**1.25**	**1,280,000**

Notes: Mineral Resources are Reported at a 0.6 g/t Au cut-off grade and ore reserves are reported based on a A$2,200 gold price as a basis for cut-off grade estimations and pit optimisations. Life of mine only includes Central zone and Dingo Resource areas. The Ore Reserve and LOM only include Measured and Indicated Resource.

For further information regarding the PFS and Maiden Ore Reserve, refer to the Executive Summary Report included in this announcement as **Appendix 1**. The Ore Reserve was prepared and reported in accordance with the *Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves* (JORC Code, 2012 edition) (the **JORC Code**). Please refer **Appendix 2** for details of the Ore Reserve.

Maiden Ore Reserve

The Project's underlying Mineral Resource is technically robust, being based on almost 234,137 m of RC and diamond drilling providing a high confidence geological model. The current mining areas are located on granted Mining Leases where small scale mining has been undertaken in the past and provides context for a large open cut mining development demonstrated within the current PFS.

The current PFS forecasts that the Project will generate A$981 million of EBITDA over the LOM and an average post-tax free cashflow during production of A$70 million a year. Over the first six years of production the Project is modelled to generate $92 million post tax free cashflow per annum during production. This projected cashflow underpins an outstanding internal rate of return of 40.7% (post tax) and a payback period of just 1.7 years required to payback expected pre-production capital expenditure. Ausgold's forecast strong financial performance is based upon an annual production rate of 126,000oz per annum and an all-in sustaining cost (AISC) of $1,370/oz for the first six years of production. The maiden Probable Ore Reserve is 32Mt at 1.25 g/t for 1.28 Moz gold.

The Project also has significant growth potential, with new drilling and additional high-grade mineralisation identified after the May 2022 Resource upgrade (ASX Announcement 25 May 2022).

Current mining studies have considered the economics at a 0.6 g/t Au cut-off grade. It was noted at current economics lower grade ore is economic (>0.4 g/t Au) which realises a larger Resource base beyond the current PFS. The potential of a large mining operation at the KGP will be considered in optimisation studies over the coming months.

Summary Information material to Maiden Ore Reserve

Material Assumptions & Outcomes

Open pit mine scheduling is based on realistic mining productivity, with readily achievable mining rates and consistent material movements. This is based on a typical mining fleet for a gold mining operation in Western Australia. Pit optimisations have been conducted at a A$2,200 gold price and mine planning developed using a 0.85 Revenue Factor and will produce 1.16 Moz gold over an 11-year LOM.

Mining Method & Assumptions
An open-cut mine production plan was generated around the mining inventory which targeted 3 Mt/a of ore processing and a mining rate limitation of 33 Mt. These targets can be achieved for a mine life in excess of 10 years, excluding Inferred Mineral Resource material and applying a 0.6 g/t Au cut-off grade.

Processing Method & Assumptions
The onsite processing plant will treat a blend of oxide, transitional and fresh gold-bearing ores from the open pits at the KGP and is designed to operate at a throughput capacity of 3 Mt/a. The crushing circuit will be a conventional open circuit jaw crusher which will feed a SABC (SAG mill, ball mill and recycle crushing) comminution circuit. Gold extraction will occur through conventional gravity and Carbon in Leach (CIL) with gold recovery via electro-winning.

Metallurgical recoveries are based on recent test work which has been used to develop a recovery curve, an average recovery of greater than 90% is expected over LOM.

Cut-off Grades (CoG) are based on project economics with open pit mining optimised to a 0.6g/t Au CoG, although lower CoG >0.4 g/t Au are considered economic under the study cost assumptions.

Material Modifying Factors
A schedule of the approvals required is presented in Appendix 1, section 4.8 (Executive Summary) of this announcement.

Project Finance Estimates

The production targets and key financial estimates included within this announcement and derived from the PFS are based on the Company's Maiden Ore Reserve, established in accordance with clause 29 of the JORC Code as an economically mineable Mineral Resource. All forward-looking financial and economic statements contained within this announcement regarding the Maiden Ore Reserve rely on compliance with the parameters of JORC Code ore reserve reporting and are accordingly established on reasonable grounds.

Realisation of production targets and key financial estimates arising out of the PFS are dependent upon, and subject to, the assumption that the Company will have the necessary financial capacity to deliver those results.

The PFS estimates a funding requirement of A$225 million to cover the capital and operating costs applicable from the start of plant production to the end of plant construction and to the end of plant commissioning and the start of gold production. The Company intends to meet this funding requirement with a mixture of debt and equity which will need to be raised before construction can begin. Further, in the interim, the Company will likely require additional funds to progress the Project through to completion of a final Definitive Feasibility Study and financial investment decision. The Company anticipates that it will be able to raise such funds through further equity issues.

While noting that outstanding funding requirements are not guaranteed, the Company considers it has reasonable grounds to assume that suitable capital funding will be available. In reaching this conclusion, the Company has considered the following factors in addition to general market conditions and economics of the Project:

- the size of upfront capital expenditure required (approximately A$225m) compared to the Company's current market capitalisation, which indicates (as at the date of this announcement) an approximate 2:1 ratio of outstanding capital expenditure to current market capitalisation, which the Company considers to be a capital expenditure leverage ratio better than comparative exploration entities within the mining industry in Australia;
- the Company's current financial position, particularly including the absence of existing material debt liabilities; and
- the Company's track record of raising capital, in particular the Company's consistent record of equity support.

Management Comment

Commenting on the Maiden Ore Reserve, Ausgold Managing Director, Matthew Greentree, said:

"Ausgold is now positioned firmly on the path to becoming Australia's next mid-tier gold producer with the Katanning Gold Project delivering a large ***1.28 Million Ounce Ore Reserve*** *with excellent financial metrics demonstrating low cost, low technical risk, and a high-margin operation.*

High grade ores identified early in the mining schedule deliver, over the first six production years, 126koz of gold on average per year and help to generate $555M of after tax free cashflow to the project over this period. This early cashflow generation facilitates an early payback of the estimated $225M of pre-production capital after 21 months, sets up an impressive IRR of 40.7% and supports a debt-equity funding model.

This initial Ore Reserve confirms the Company's robust understanding of the Katanning gold deposit and further supports our thesis that this represents the foundation of an excellent mine operation with clear upside potential".

Next Steps

The Definitive Feasibility Study (DFS) with completion due late Q4 CY2023

- **Resource Drilling -** additional targeted drilling to improve confidence and further expand the current Resource. At present one diamond rig is operating at the KGP, drilling in the Central Zone testing Resource extensions. Jinkas Deeps – Planned deep drilling will target the down-plunge gold mineralisation at the Jinkas lode within the Central Zone. This new drilling is supported by several untested down-hole EM plates at 400m vertical depth, extending a further 800m north along strike.
- **Open pit mine studies are underway -** assessing potential mining scenarios, in particular further optimising open pit designs, schedules, and development strategies
- **Metallurgy -** additional sampling from diamond drill core for comminution and leach testwork over the range of ore types
- **Process Design -** flow sheet optimisation following metallurgical testwork results and analysis; confirmation of mechanical equipment list and electrical load list; cost models; execution strategy
- **Tailings Storage Facility (TSF) -** tailings testwork to confirm chemical and physical properties; optimisation of TSF design, geotechnical site investigation
- **Hydrogeology -** groundwater investigation and modelling to determine pit dewatering and confirm process water supply solution
- **Infrastructure -** complete feasibility study to confirm connection to grid and investigate optimisation of Renewable Energy contribution to the power supply; determine bore field location for process water supply; investigate and confirm accommodation for construction and operations; determine site access and intern roads designs
- **Environmental -** additional baseline studies within the Project's disturbance envelope; moving toward completion of the Environmental Review Document
- **Community -** on going Stakeholder Engagement Programs; establishment of Project Office in Katanning; employment opportunities; community response surveys;

About Ausgold Limited

Ausgold Limited (ASX: AUC) is a gold exploration and development company based in Western Australia.

The Company's flagship project is the Katanning Gold Project, located 275km south-east of Perth and approximately 40km north-east of the wheatbelt town of Katanning. Ausgold holds a dominant ground position in this relatively underexplored greenstone belt, an area prospective for Archean gold deposits. The current Resource at Katanning is 2.16 Moz gold (Table 3).

Ausgold's portfolio also includes the Doolgunna Station Cu-Au project and the Yamarna Ni-Cu-Co project in Western Australia and the Cracow Au Project in Queensland.

Table 3 - Current Mineral Resource
(details in ASX release 25 May 2022)

	Tonnes (Mt)	Grade (g/t)	MOz Gold
Measured	19.0	1.31	0.80
Indicated	26.8	1.14	0.98
Inferred	9.5	1.03	0.37
Total	**56.0**	**1.21**	**2.16**

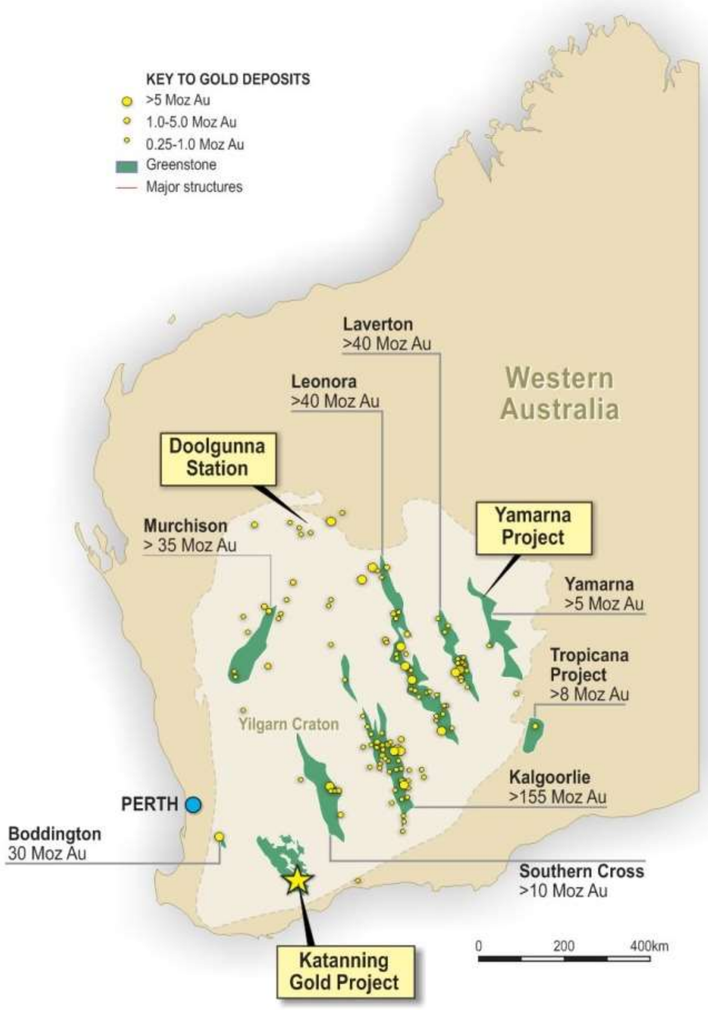

Figure 1 - Regional map showing the KGP, other Ausgold projects and mineralised greenstone belts

The information in this report that relates to the Mineral Resource in Table 3 is based on information announced to the ASX on 25 May 2022. Ausgold confirms that it is not aware of any new information or data that materially affects the information included in the relevant market announcement and that all material assumptions and technical parameters underpinning the estimates in that announcement continue to apply and have not materially changed.

The Board of Directors of Ausgold Limited approved this announcement for release to ASX.

On behalf of the Board
MATTHEW GREENTREE
Managing Director
Ausgold Limited

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Competent Persons' Statements

The information in this statement that relates to the Mineral Resource estimates is based on work carried out by Dr Michael Cunningham of Sonny Consulting Services Pty Ltd, Mr Daniel Guibal of Condor Geostats Services and Dr Matthew Greentree of Ausgold Limited in 2021 and 2022. The information in this statement that relates to the Ore Reserve estimates is based on work carried out by Mr Andrew Hutson of Resolve Mining Solutions in 2022.
Dr Greentree is Managing Director and a shareholder in Ausgold Limited. Dr Greentree takes responsibility for the integrity of the Exploration Results, including sampling, assaying, QA/QC, the preparation of the geological interpretations, and Exploration Targets. Dr Michael Cunningham is an option holder in Ausgold Limited and takes responsibility for the Mineral Resource estimates for the Jackson, Olympia, Dingo and Datatine deposits. Mr Daniel Guibal takes responsibility for the Mineral Resource estimates for the Jinkas and White Dam deposits.

Dr Cunningham, Mr Guibal and Dr Greentree are Members of the Australasian Institute of Mining and Metallurgy and have sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration, and to the activity they are undertaking, to qualify as Competent Persons in terms of the *Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves* (JORC Code, 2012 edition).

Mr Hutson is a Fellow of the Australasian Institute of Mining and Metallurgy and has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration, and to the activity they are undertaking, to qualify as Competent Persons in terms of the *Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves* (JORC Code, 2012 edition).

The Competent Persons consent to the inclusion of such information in this report in the form and context in which it appears.

Forward-Looking Statements

This announcement includes 'forward-looking statements' as that term is understood the meaning of securities laws of applicable jurisdictions. Forward-looking statements involve known and unknown risks, uncertainties and other factors that are in some cases beyond Ausgold Limited's control. These forward-looking statements include, but are not limited to, all statements other than statements of historical facts contained in this presentation, including, without limitation, those regarding Ausgold Limited's future expectations. Readers can identify forward-looking statements by terminology such as 'aim', 'anticipate', 'assume', 'believe', 'continue', 'could', 'estimate,' 'expect', 'forecast', 'intend', 'may', 'plan', 'potential', 'predict', 'project', 'risk', 'should', 'will' or 'would' and other similar expressions.

Risks, uncertainties and other factors may cause Ausgold Limited's actual results, performance, production or achievements to differ materially from those expressed or implied by the forward-looking statements (and from past results, performance or achievements). These factors include, but are not limited to, the failure to complete and commission the mine facilities, processing plant and related infrastructure in the timeframe and within estimated costs currently planned; variations in global demand and price for commodities; fluctuations in exchange rates between the US dollar and the Australian dollar; the failure of Ausgold Limited's suppliers, service providers and partners to fulfil their obligations under construction, supply and other agreements; unforeseen geological, physical or meteorological conditions, natural disasters or cyclones; changes in the regulatory environment, industrial disputes, labour shortages, political and other factors; the inability to obtain additional financing, if required, on commercially suitable terms; and global and regional economic conditions. Readers are cautioned not to place undue reliance on forward-looking statements.

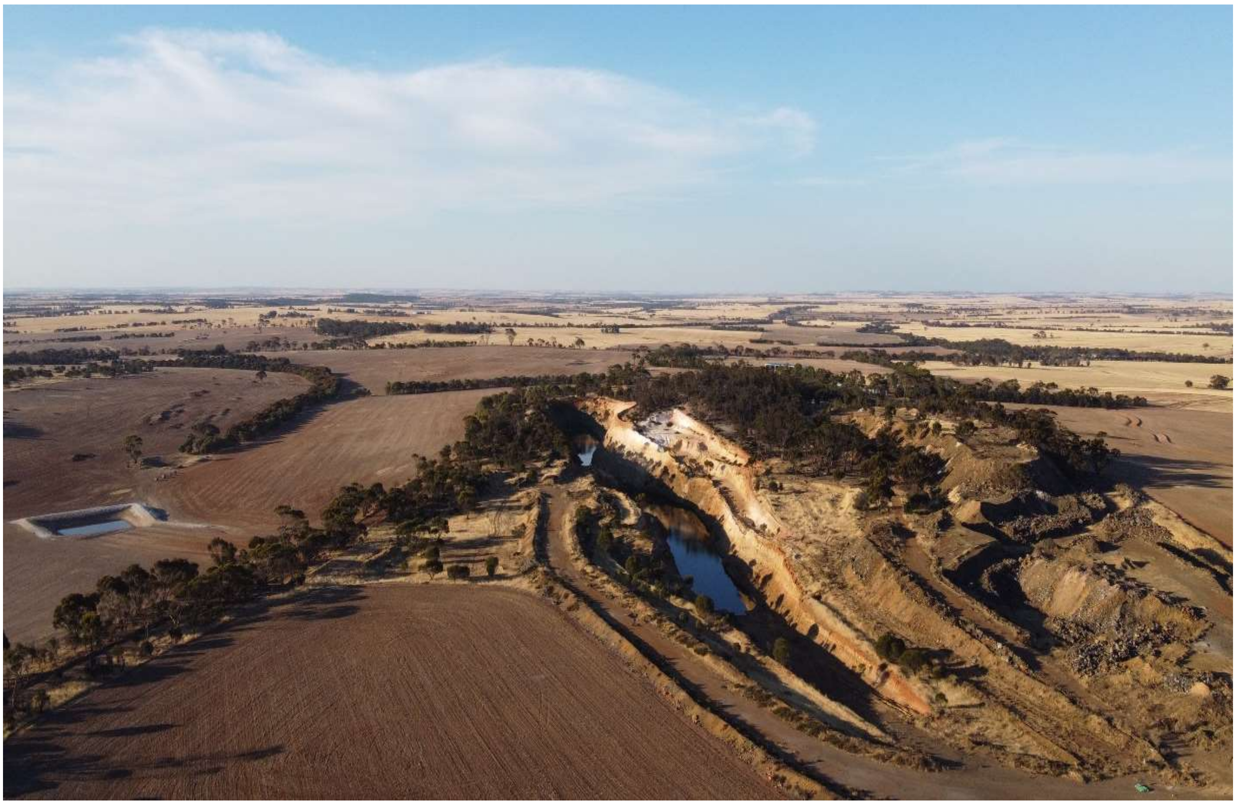
The information concerning possible production in this announcement is not intended to be a forecast, but relates to internally generated goals set by the Board of Directors of Ausgold Limited. Ausgold's ability to achieve any targets will be largely determined by its ability to secure adequate funding, implement mining plans, resolve logistical issues associated with mining and enter into any necessary offtake arrangements with reputable third parties. Although Ausgold Limited believes that the expectations reflected in these forward-looking statements are reasonable, such statements involve risks and uncertainties, and no assurance can be given that actual results will be consistent with these forward-looking statements.

Currency and Cost Assumptions

All financial amounts in this report are expressed as Australian dollars as either 'A$' unless otherwise indicated. Costs have been estimated in Q2 2022 Australian dollars and are not escalated or inflated. Cashflow discounting begins after construction and during the ramp-up period.

APPENDIX 1 – EXECUTIVE SUMMARY

Katanning Gold Project
Prefeasibility Study



Executive Summary Report – August 2022

KGP Prefeasibility Study Contributors

Resolve Mining Solutions – Pit Optimisations, Mine Schedules and Mine Designs

GR Engineering Services Limited (GRES) – Comminution Modelling, Processing Plant Design and Cost Estimates, Execution Planning

Knight Piésold Consulting – Tailings Storage Facility Design and Cost Estimation

SRK Consulting – Hydrogeology

NorthShore Capital Advisors – Financial Modelling

ALS Laboratories – Metallurgical Testwork

Preston Consulting – Environmental Approvals Planning

OreTeck Mining Solutions – Mine Geotechnical Engineering

WSP Golder – Stakeholder Engagement and Analysis

Sonny Consulting – Mineral Resource Estimation

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List of Abbreviations

3D	three-dimensional
A$	Australian dollars
AARL	Anglo American Research Laboratories
ASX	Australian Securities Commission
Au	chemical symbol for gold
CIL	carbon-in-leach
CY	calendar year
ENE	east-northeast
EPC	engineering-procurement-construction
GRES	GR Engineering Services Limited
HDPE	high density polyethylene
HV	high voltage
IPP	independent power production
IRR	internal rate of return
JORC	Joint Ore Reserves Committee
KGP	Katanning Gold Project
LOM	Life of Mine
MGA94	Map Grid of Australia 1994
MSA	mine service area
NNE	north-northeast
NNW	north-northwest
NPV	net present value
PFS	prefeasibility study
Q1	Quarter 1
Q2	Quarter 2
QA/QC	quality assurance and quality control
ROM	run-of-mine
SABC	SAG milling, ball milling and crushing
SAG	semi-autogenous grinding
SMU	selective mining unit
SSE	south-southeast
TSF	tailings storage facility
WNW	west-northwest

Units of Measurement

µm	microns
A$/t	Australian dollars per tonne
dt/h	dry tonnes per hour
g/t	grams per tonne
ha	hectares
km	kilometres
koz	kilo-ounces
kW	kilowatts
m RL	metres reduced level
m	metres
m^2	square metres
m^3	cubic metres
m^3/d	cubic metres per day
mm	millimetres
Mt	million tonnes
Mt/a	million tonnes per annum
t/d	tonnes per day

1. Project summary

The Katanning Gold Project (KGP, Project) Prefeasibility Study (PFS) describes a technically and economically robust project in the Great Southern region of Western Australia. Its location in an agricultural region only 3.5 hours' drive from Perth provides ready access to a skilled workforce, existing infrastructure and supporting services.

The PFS underpins a maiden Ore Reserve of 32.0 Mt grading at 1.25 g/t Au, and describes a Life of Mine (LOM) plan which initially extends over a 11-year period and produces 105 koz per annum. The current project demonstrates excellent key financial metrics including a LOM revenue of A$2.67 billion and a net present value (NPV) after tax of A$364 million. High grades in the initial six years of production deliver, on average per year, 126 koz of gold and A$92 million of undiscounted cashflow after tax, which contributes to an early payback of 1.7 years and a post-tax IRR of 40.7%.

The PFS is based on the Mineral Resource estimate completed in May 2022, and drilling continues to delineate further extensions to gold mineralisation through exploration success.

2. Key Life of Mine highlights

Key study outcomes:

- LOM revenue of A$2.67 billion and post-tax undiscounted free cashflow of A$540 million
- Payback period of 1.7 years
- Internal rate of return of 40.7% post-tax
- Large 2.16 Moz Mineral Resource, still open to the north and south
- Impressive conversion to a 1.3 Moz Maiden Ore Reserve
- Annual production of 105 koz per annum for a 11-year LOM with significant extension opportunity
- Project on freehold land with existing Mining Leases over mining areas
- Proximity to Katanning and neighbouring communities with available services, existing access and infrastructure, accommodation, and labour force
- Able to draw additional resources from Perth (3.5 hours' drive) and Albany (2 hours' drive)
- Community support for the KGP, recognising an opportunity for economic diversity, training and job creation
- Viable connection to power grid with increasing renewable energy proportion (REP)
- 100% project ownership by Ausgold
- Small environmental impact, little clearing required
- Unlocking a new Mineral Resource area in WA's Great Southern region.

3. Project setting

The KGP is in the Great Southern region 350 km southeast of Perth and 35 km northeast of the wheat and sheep farming town of Katanning. The KGP can be accessed by a combination of sealed roads and gravel roads. The majority of Ausgold's tenement holdings lie on freehold land.

The KGP gold mineralisation extends along a strike length of 7.5 km. The PFS is based on an estimated Mineral Resource (Measured, Indicated and Inferred) of 56 Mt grading at 1.21 g/t Au.

The gold mineralisation was first identified in 1979 by Otter Exploration NL. After several owners, International Mineral Resources NL commenced mining in December 1995 at what was then called the Badgebup Project, focusing on the Jinkas and Dingo Hill resource areas. International Mineral Resources NL had purchased the leases and the Grants Patch treatment plant from Glengarry Mining NL. Processing commenced in January 1996 and ceased in July 1997. A total of 302,000 tonnes of mostly oxide ore, at an average grade of 2.54 g/t Au was milled, with 20,000 ounces of gold produced.

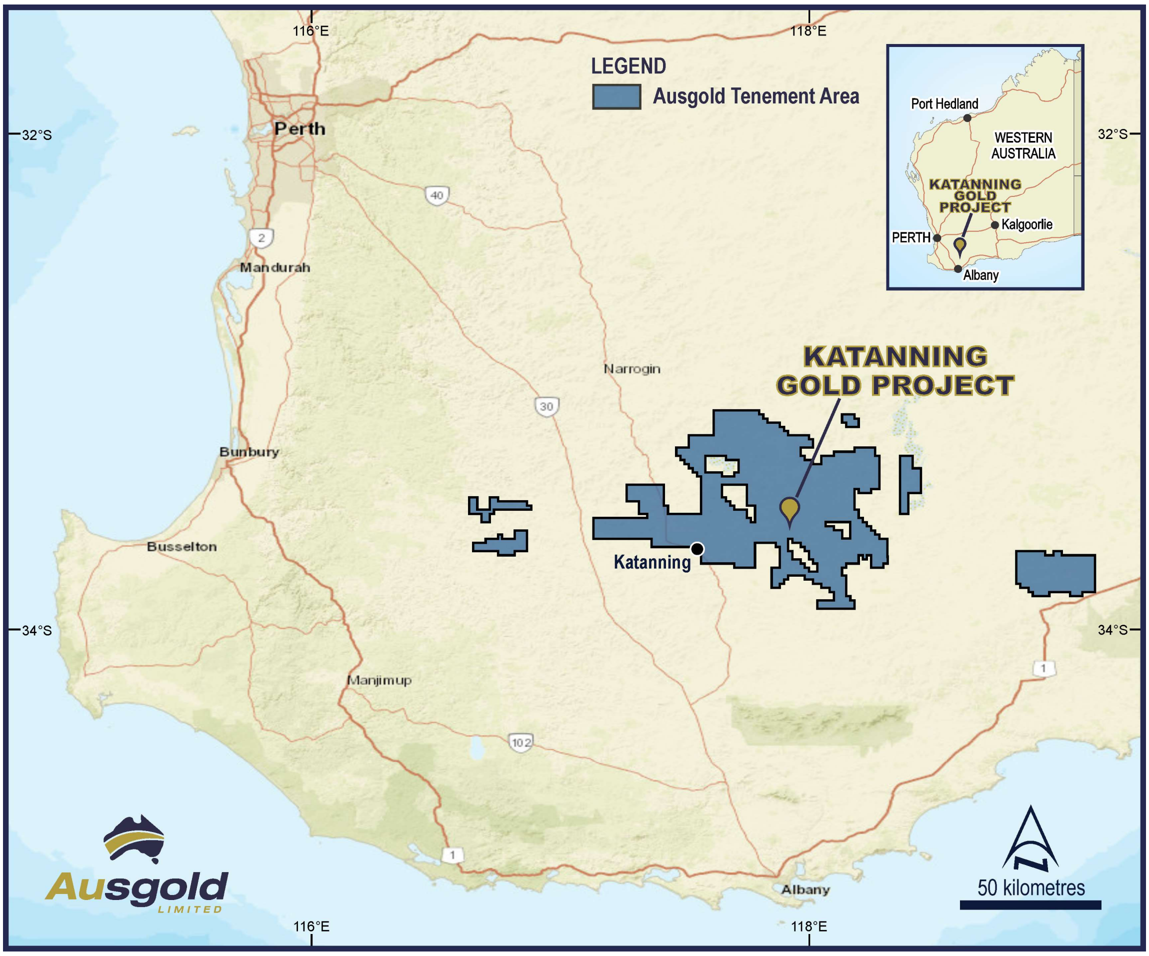

Figure 1: Project location map

4. Project details

4.1 Geological setting

The gold mineralisation at the KGP is localised along its eastern boundary by a regionally significant thrust fault-bound block which extends over at least 17 km of strike length. Thrust faults also define the eastern and western boundaries of the rocks hosting the gold mineralisation. The gold mineralisation is localised into three laterally continuous lodes which extend for over 7 km of strike length. These lodes are defined from the west to east as the Jackson–Dingo lode, White Dam lode and Jinkas lode.

The mineralised lodes contain shallowly plunging high-grade ore shoots which are interpreted as fold axes of the tightly folded and metamorphosed mafic host rocks. The overall KGP is broadly folded along an east–west axis. The gold mineralisation on the northern limb (Central Zone) plunges 18° towards the NNE. This plunge reverses on the southern limb (Southern Zone), plunging 9° towards the SSE.

The mineralised lodes follow the gneissic foliation, with mineralisation being correlated between holes and drill sections following this trend. Geological logging of drill holes has been used to interpret major geological boundaries and develop a 3D geological model. Wireframing of the gold mineralisation (>0.3 g/t Au) was based on drill hole data and honoured the geological boundaries.

Mineral Resource estimates are reported using a 0.6 g/t Au cut-off grade and reporting has been limited to a depth of approximately 150 m below surface.

4.1.1 Gold mineralised lodes

The gold mineralisation occurred in separate lodes folded around a quartz monzonite sill separating gold mineralisation. The most significant in terms of contained ounces is the Jinkas–White Dam lode, representing a single folded lode. The Jinkas lode is reported above the quartz monzonite and White Dam lode below the quartz monzonite. The quartz monzonite is interpreted to have intruded during peak metamorphism and after mineralisation. The quartz monzonite forms the core of a major tight WNW-plunging synform; it follows the northerly plunge and extends over a 4,200 m strike length. It is thickest at the Olympia resource area and thins towards the south, to the Rifle Range prospect where it is eroded at surface.

Jinkas has one primary lode adjacent to the quartz monzonite and 25 defined secondary subparallel lodes, striking NNW and dipping at approximately 35° to the ENE. The Jinkas lode is defined along a 3,300 m strike length and extends 480 m down dip. The primary Jinkas lode is between 10 m and 25 m thick and the secondary lodes are on average between 3 and 5m thick.

White Dam consists of the hangingwall lode, which is the folded continuation of the Jinkas footwall lode. Two additional lodes lie approximately 20 m beneath the main hangingwall lode and 30–50 m above the Jackson lodes. The revised model connects the White Dam and Jinkas lodes through the thickened Jinkas South fold hinge position, which extends over a strike length of approximately 3,300 m. The primary White Dam lode is between 10 m and 25 m thick and the secondary lodes are between 3 m and 5 m thick.

The Mineral Resource estimates for Jinkas–White Dam were prepared from a total of 26,195 lode composites from 1,147 drill holes. Drill spacing is variable and ranges from 20 m to 40 m along section lines at a spacing of 20–80 m. The dataset comprises a mix of shallow vertical holes (mainly on the western side of the deposit) and deeper holes angled at 60° towards 244°.

The Mineral Resource estimates for the **Olympia** deposit were first reported in the 2018 Mineral Resource announcement. Drilling to the north, along strike from Jinkas, has demonstrated continuity between the two deposits, despite some displacement from interpreted strike-slip faults.

Interpretation of a revised model consisting of 24 mineralised lodes extending over a strike of 1,500 m shows mineralisation remains open along strike to the south and north. The Mineral Resource estimates were prepared from a total of 902 (1 m) lode composites from 118 drill holes, where drill spacing is variable and ranges from 30 m to 100 m along 20–100 m spaced section lines. This included 246 new lode composites from 36 drill holes completed since the December 2021 model update. Most holes are angled at 60° towards 244°.

Jackson consists of 32 subparallel lodes striking to the NNW and dipping at approximately 30° to the ENE. The Jackson lodes are located approximately 30–50 m below the White Dam lodes. The Jackson lodes have defined strike lengths up to 5,000 m and dip extents ranging from 285 m to 624 m. Lode thicknesses average between 3 m and 5 m. The lodes have been interpreted from the surface to a depth of 160 m.

The Mineral Resource estimate for Jackson was prepared from a total of 5,137 (1 m) lode composites from 1,665 drill holes. This included 791 new lode composites from 138 drill holes completed since the December 2021 model update. Hole spacing is variable and ranges from 20 m to 60 m along 30–120 m spaced drill lines. The dataset comprises a mix of shallow vertical holes (mainly in the southern half and on the western side of the deposit), and deeper holes angled at 60° towards 244°.

The Mineral Resources for the **Dingo** deposit were re-estimated based on a revised geological and mineralisation model derived from new drilling. The estimates were prepared from a total of 8,946 (1 m) lode composites from 457 holes, including 47 new holes with 929 (1 m) composites. The Dingo deposit occurs as a standalone deposit in the Southern Zone of the KGP, extending over 1,900 m of strike and dip extents ranging from 220 m to 420 m. In all, 16 mineralised lodes were interpreted. The average lode thickness is approximately 5 m.

4.2 Mineral Resource

The estimation of Mineral Resources was conducted in accordance with industry best practice for gold resource estimation and the Mineral Resources were classified in accordance with the guidelines of the 2012 edition of the *Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves* (JORC Code 2012). The Mineral Resource estimate was released to the Australian Securities Exchange in May 2022.

The geological models were revised using new geoscientific information collected during the exploration campaigns completed up to March 2021. Wireframes of gold mineralisation >0.3 g/t Au and major geological units were developed by Ausgold and Sonny Consulting.

A Mineral Resource Statement is given in Table 1. Sections 1–3 of the JORC Code Table 1 are included (Ausgold's ASX Announcement of 25 May 2022).

A mining block model was produced to estimate internal dilution for the Ore Reserves (blocks of 2.5 m by 2.5 m by 2.5m).

The primary changes were as follows:

- Samples were composited to 2.5 m to match bench heights.
- Top-cuts changed on 2.5 m composites to the following:
    - *Jinkas/White Dam hangingwall top-cut: 42 g/t Au (*a further spatial distance restriction – 15 m at 30 g/t Au – was applied to the high-grade samples)

  - Jackson/White Dam top-cut: 12 g/t Au
  - Olympia top-cut: 6 g/t Au
  - Dingo top-cuts: 14 g/t Au.
- Variogram models changed for 2.5 m composites.
- Block model selective mining unit (SMU) changed from 10 m by 10 m by 1 m to 10 m by 10 m by 2.5 m.
- Estimates for Olympia and Jackson were obtained by conventional proportional block modelling using Ordinary Kriging.
- Estimates for Dingo and Jinkas–White Dam were obtained by using Uniform Conditioning on panels of 10 m by 10 m by 2.5 m. As a result of the Uniform Conditioning process, grade-tonnage curves of 2.5 m by 2.5 m by 2.5 m SMUs were obtained for each panel. Using a technique called Localised Uniform Conditioning (LUC), individual SMUs were then determined within each panel.

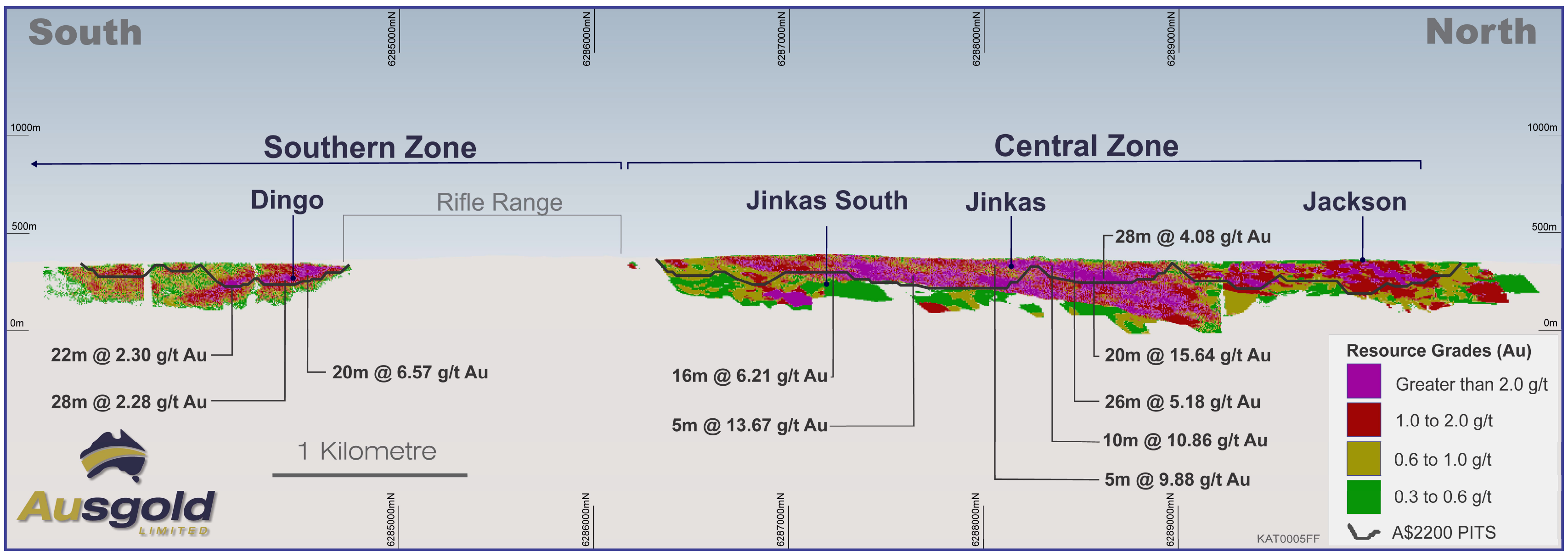

Figure 2: Long section looking west through KGP Resource with the designed PFS A$2,200 pits

Table 1: Mineral Resource estimates as at 25 May 2022

Material	Cut-off grade (g/t Au)	Measured			Indicated			Inferred			Total		
		Tonnes	Grade (g/t Au)	Ounces	Tonnes	Grade (g/t Au)	Ounces	Tonnes	Grade (g/t Au)	Ounces	Tonnes	Grade (g/t Au)	Ounces
Oxide		613,000	1.13	22,000	1,729,000	1.00	56,000	97,000	1.01	3,000	2,441,000	1.04	83,000
Transitional	0.6	2,790,000	1.46	131,000	3,877,000	1.07	134,000	107,000	1.11	4,000	6,773,000	1.23	267,000
Fresh		15,636,000	1.29	647,000	21,235,000	1.16	794,000	8,671,000	1.09	297,000	45,341,000	1.22	1,739,000
Fresh - Underground	1.8							560,000	3.25	59,000	560,000	3.25	59,000
Tailings	0							870,000	0.35	9,730	870,000	0.35	9,730
Total		**19,039,000**	**1.31**	**800,000**	**26,841,000**	**1.14**	**984,000**	**9,540,000**	**1.03**	**370,000**	**55,980,000**	**1.21**	**2,160,000**

Notes: The Mineral Resource is reported at a lower cut-off grade of 0.6 g/t Au and above 150 m RL (approximately 220 m depth). The underground Mineral Resource is reported at a 1.8 g/t Au cut-off grade and beneath 150 m RL. Figures may not sum due to rounding.

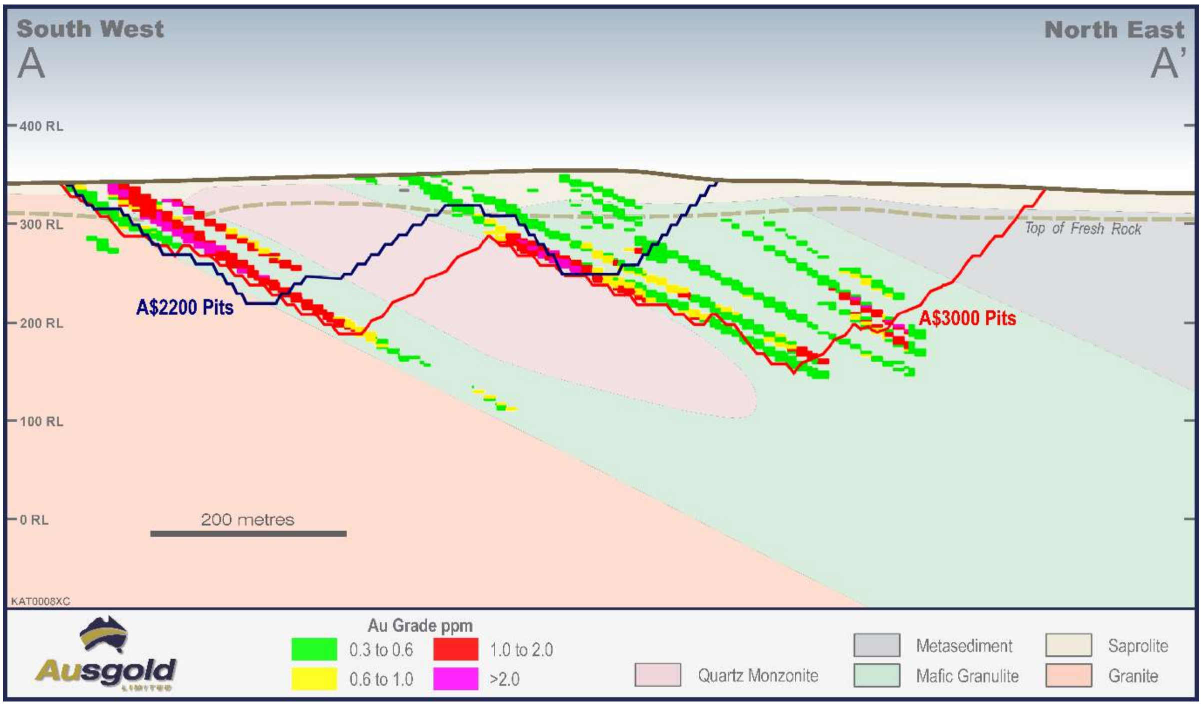

Figure 3: Jackson and Olympia North cross-section A-A', looking north

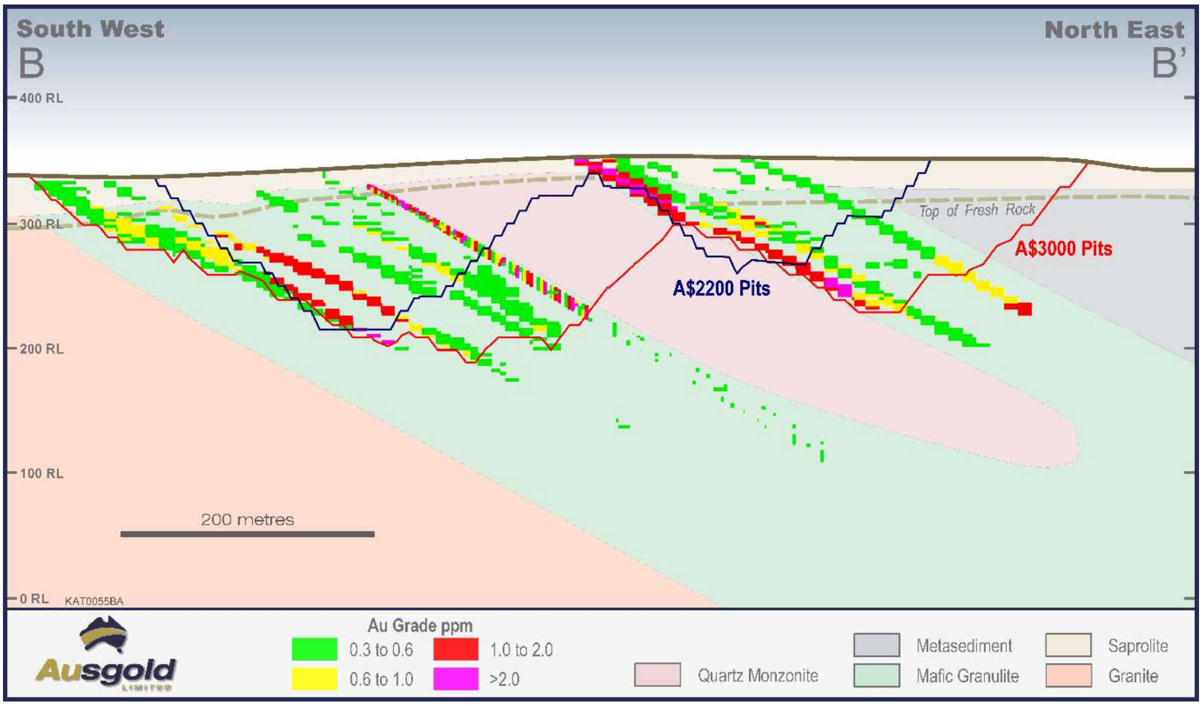

Figure 4: Jackson and Olympia South cross-section B-B', looking north

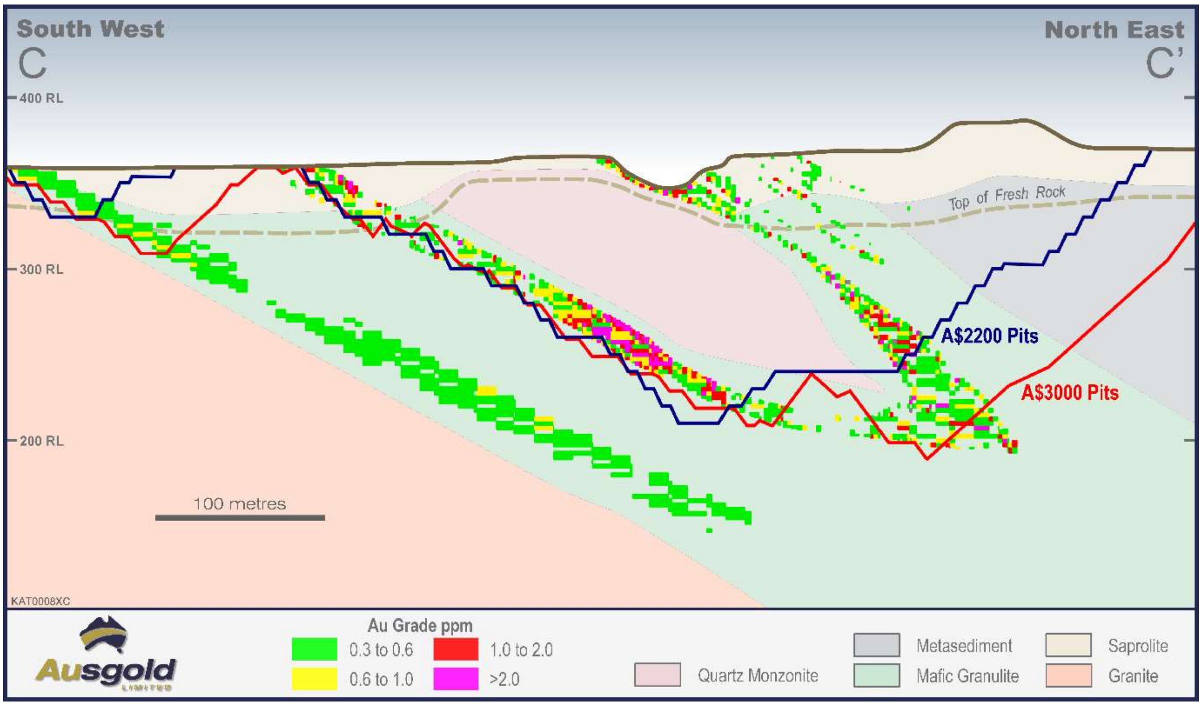

Figure 5: Jinkas cross-section C-C', looking north

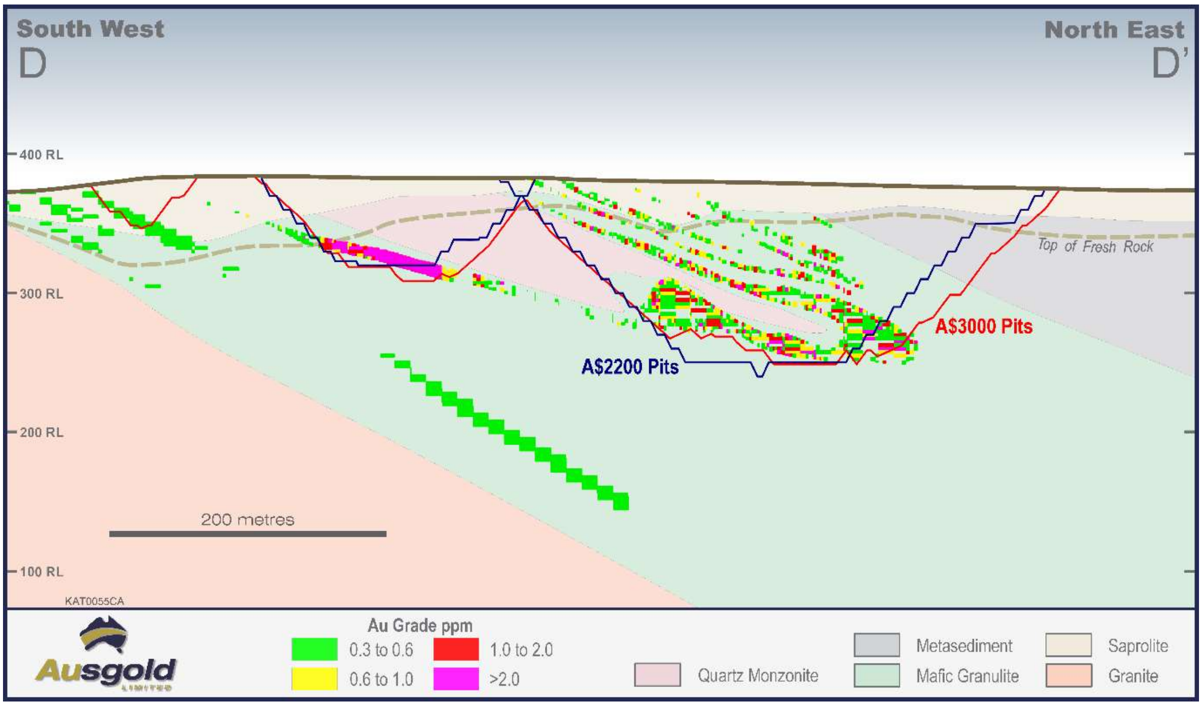

Figure 6: Jinkas South cross-section D-D', looking north

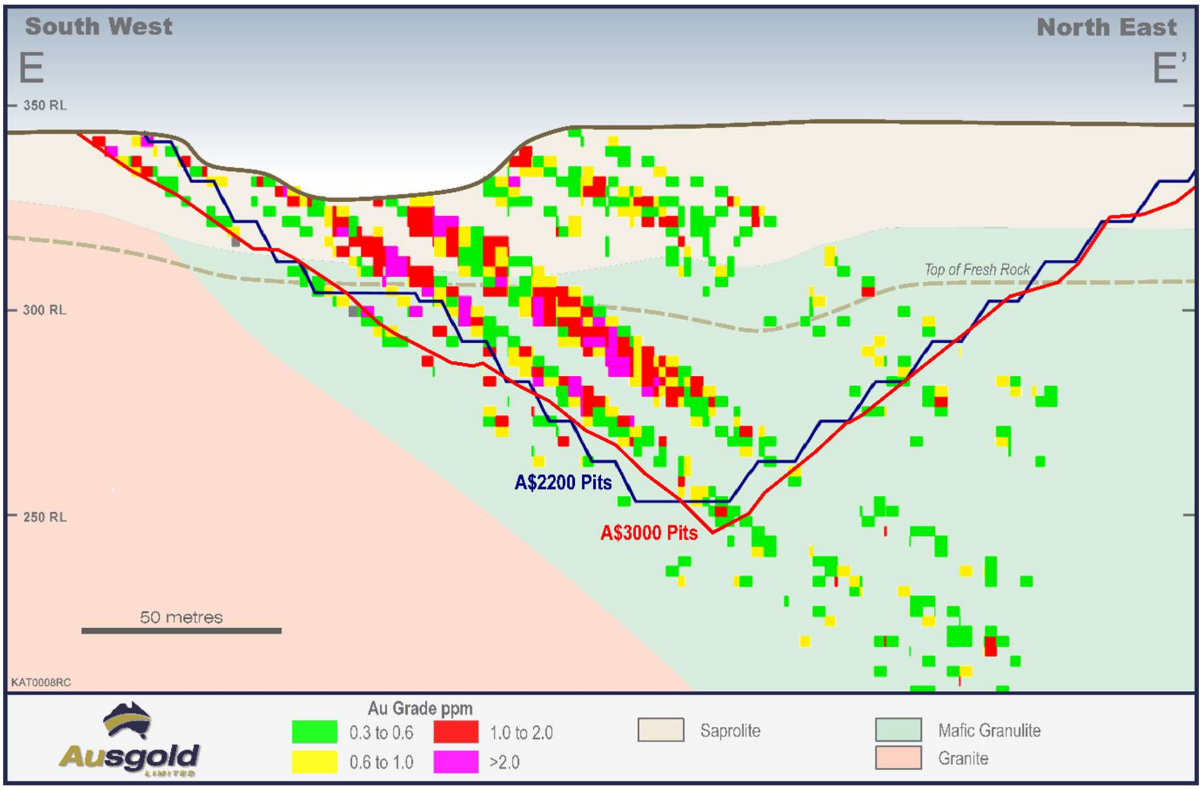

Figure 7: Dingo South cross-section D-D', looking north

4.3 Mining and Ore Reserve

The Project will be mined by open pit mining methods using conventional mining equipment. The final pit design is based on the Ore Reserve. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement, minimise rates of vertical mining advance, utilise planned processing plant capacity and expedite free cash generation – all in a safe manner.

The open pit scheduling is based on realistic mining productivity, with readily achievable mining rates and consistent material movements. The mining operating costs are based on contractors' budgeted quotes for drilling, blasting, loading and haulage, and were reviewed using first principles.

4.3.1 Geotechnical assessment

Seven diamond drill holes for a total of 794.5 m were completed between September and December 2021 to collect geotechnical data and select samples for testing. Planning for diamond drill hole locations was based on the August 2021 Mineral Resource model and conceptual open pit designs. Geotechnical logging of each drill hole was completed by the Company's geologists under the direction of the geotechnical engineer who was on site prior to and during the drilling and logging program. In addition, downhole televiewer logging was completed on nine diamond drill holes and three reverse circulation holes advanced for exploration and metallurgical testwork sampling. The exploration geologists and geotechnical engineer carried out structural mapping on the exposed walls of the Jinkas pit.

The geotechnical engineer also provided direction during selection of samples for laboratory testwork, ensuring there was an adequate number of samples across each geotechnical (soil/rock mass) unit. A total of 170 samples were selected and delivered to the geotechnical testing laboratory in Perth.

The geotechnical engineer collated and analysed the logging data and testwork results to determine pit slope design parameters, specifically inter-ramp angles as a function of bench design angles, bench heights and berm widths. These parameters were used for the pit optimisation and pit designs.

4.3.2 Pit optimisation

Whittle open pit optimisations were completed using the resource model created by Ausgold. The model was built with block dimensions approximating an SMU of 2.5 m by 2.5 m by 2.5 m and therefore includes sufficient dilution and ore loss for this level of study. The modifying factors used in the optimisations are summarised in the JORC Code Table 1 and were developed by Ausgold and its study team.

Pit optimisation, excluding Inferred Mineral Resource material and applying a 0.6 g/t Au cut-off grade, produced a pit shell containing 36.5 Mt of mill feed at an average grade of 1.30 g/t Au, as shown in Figure 8.

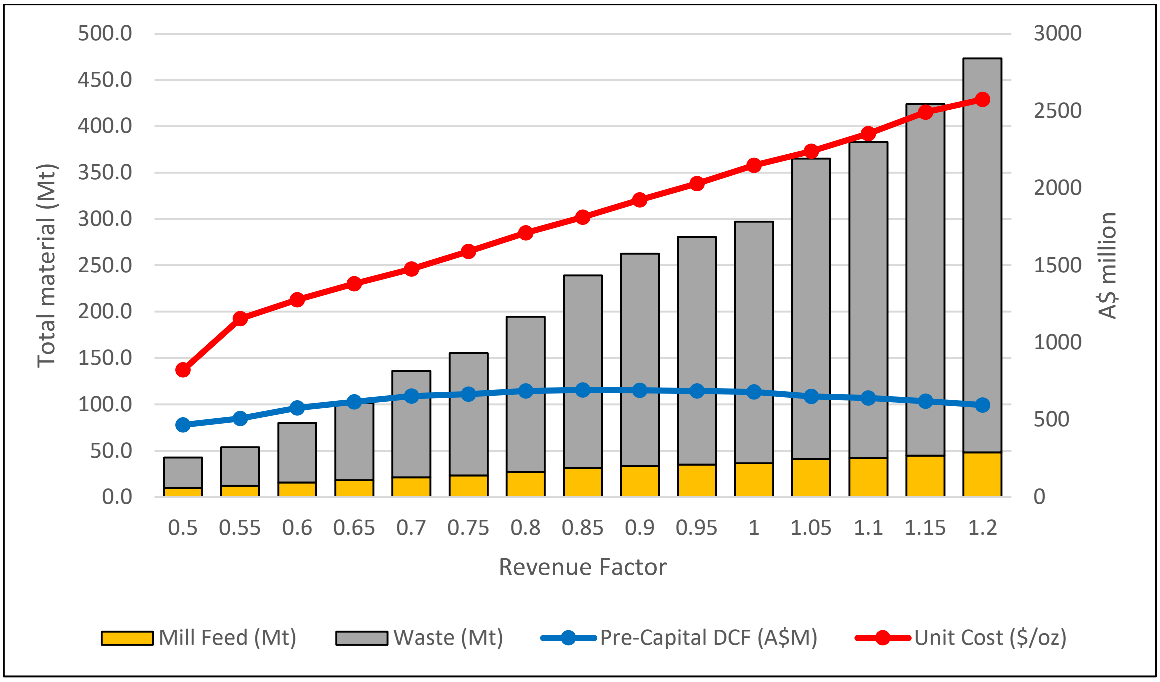

Figure 8: Optimisation results

Pit shell selection considered both the overall project value and the current design capacity of the tailings storage facility (TSF). Based on this, the 0.85 revenue factor (RF=0.85) pit shell was selected for the pit design; however, the larger RF=1 pit shell was also used to ensure that no additional potential ore was sterilised at this early phase of development.

Consideration of the RF=1 pit shell also provides a potential upside case should the current design limitations on the TSF be lifted.

4.3.3 Mine designs and schedule

Pit designs have resulted in a near-continuous pit over a 4.5 km strike length with only a few breaks between the Olympia and Jinkas deposits. Designs have been completed to include pit staging to allow access to early higher grades around the main Jinkas deposit, then cutbacks to access the deeper ores later in the mine life. The final pit design also allows for multiple mining areas, which is favourable for managing ore blending and timing of development activities.

Waste dumps were located adjacent to the pit, on the western side, but allowing access to be maintained along most of the existing roads. The dump locations also take the requirements to supply waste for the tailings dam construction and preserve the remnant native bushland into consideration. Sufficient volume has been designed for all the waste mined, inclusive of a 25% swell factor.

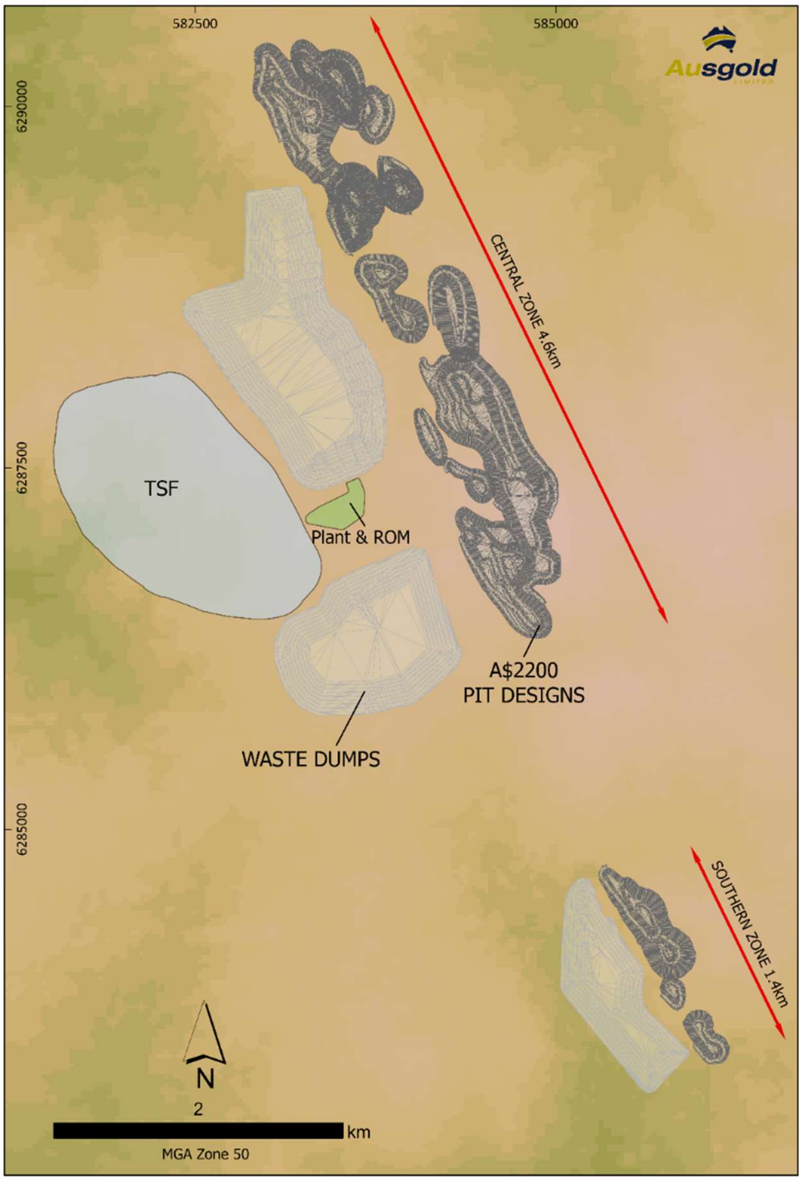

Figure 9: Site layout plan

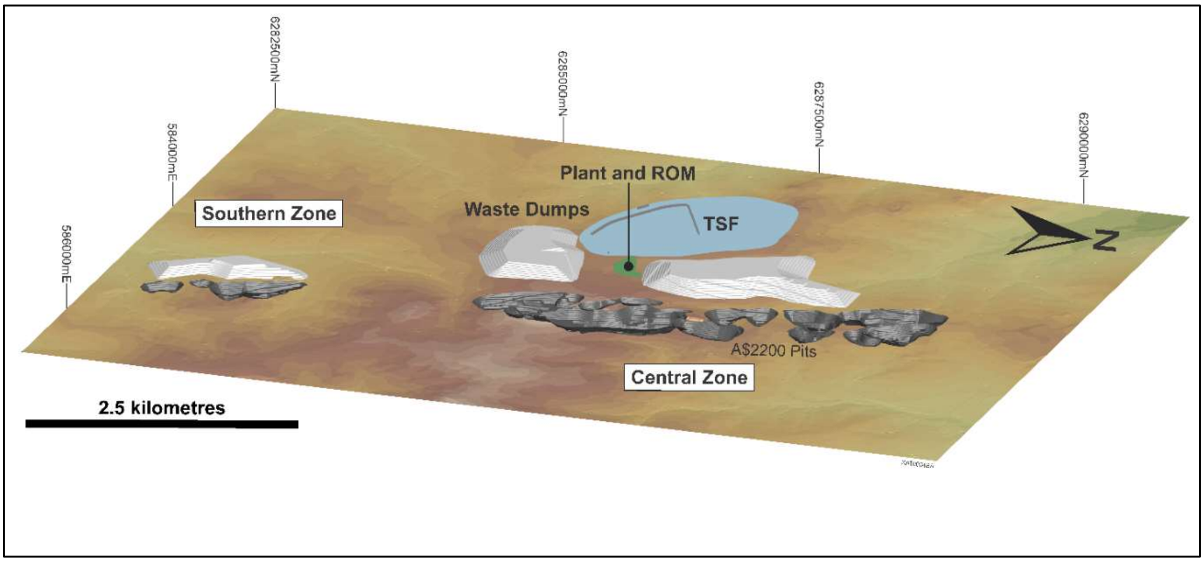

Figure 10: Oblique view looking southwest (-25/240°) of the site plan

A production plan was generated around the mining inventory which targeted 3.0 Mt/a of ore processing and a mining rate limitation of 33 Mt/a. These targets can be achieved for a mine life in excess of 10 years.

The production schedule is shown in Figure 11 and Figure 12 for mining and processing, respectively.

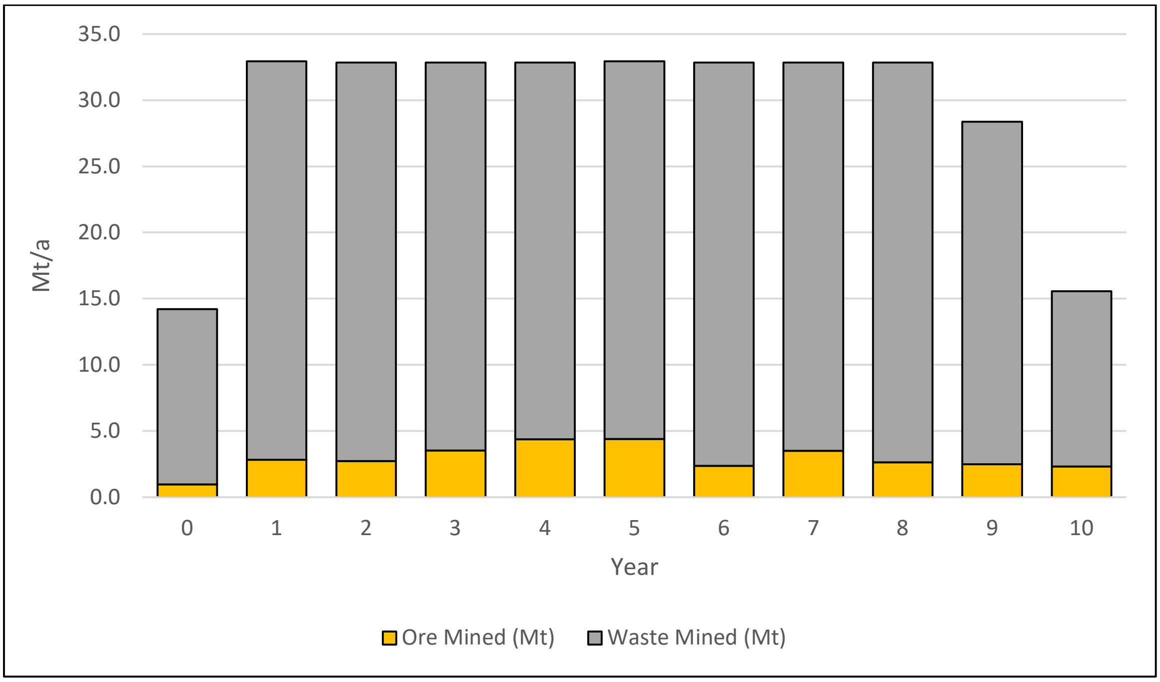

Figure 11: Annual mining plan

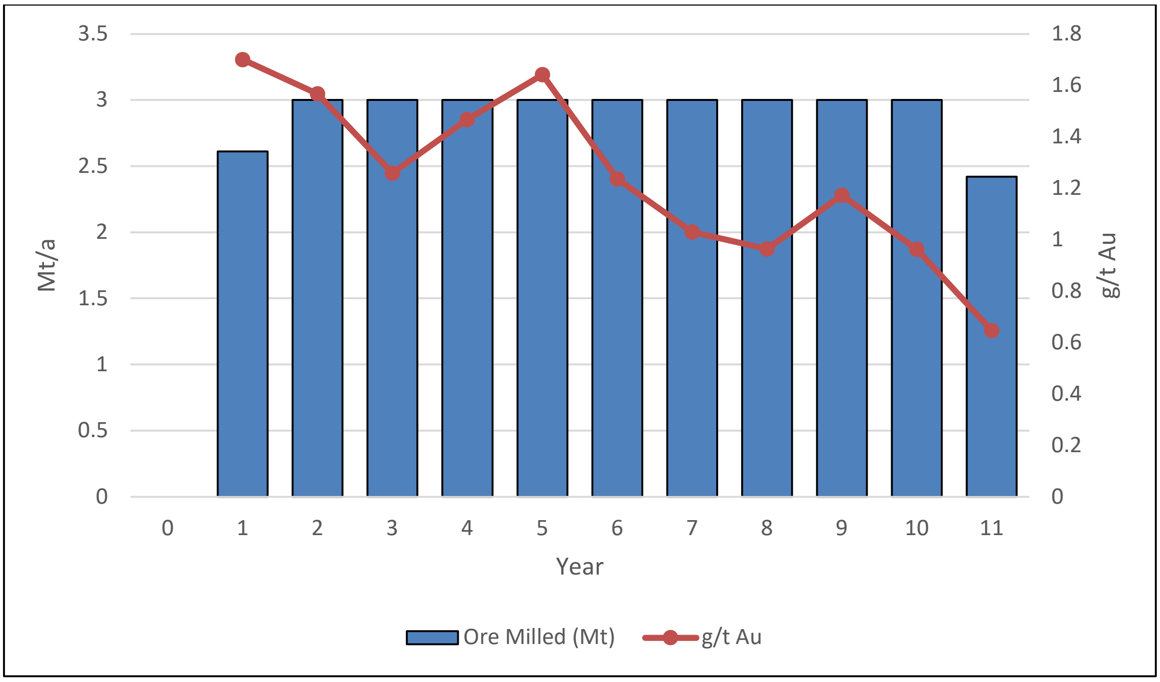

Figure 12: Annual processing plan

The schedules show that a fleet of three 150–200 tonne class excavators can meet the production rate required. These excavators are well matched to 100–135 tonne capacity trucks, with a fleet likely to consist of between 10 and 12 trucks.

This production plan can achieve the 3.0 Mt/a milling rate. This is based on a mining rate that requires a vertical advance rate of less than 20 m per annum per pit, which should be achievable with an efficient mining crew.

4.3.4 Maiden Ore Reserve

The study has produced a maiden Ore Reserve estimate prepared under the guidelines of the 2012 JORC Code of 32.0 Mt grading at 1.25 g/t Au for 1,280,000 oz of gold across all deposits at the KGP. The Ore Reserve is based on the updated 2022 Mineral Resource estimate (Ausgold's ASX release of 25 May 2022) of 56 Mt grading at 1.21 g/t Au for 2.16 Moz.

The Ore Reserves are estimated from their respective Mineral Resources after consideration of the level of confidence in the Mineral Resource and taking account of material and relevant modifying factors. As there is still further engineering work to be undertaken with respect to the TSF capacities and geotechnical review, the Ore Reserve has been classified as Probable for this level of study. It is expected that a Proved Ore Reserve will be achieved in the next stage of development. No Inferred Mineral Resources have been included in the Ore Reserve.

A summary of the data and methodologies supporting the Mineral Resource estimates form part of this ASX release, including JORC Code Table 1 (Appendix 1).

Table 2: Maiden Ore Reserve estimate as at 1 August 2022

Proved Ore Reserves			Probable Ore Reserves			Total Ore Reserves		
Tonnes (Mt)	Grade (g/t Au)	Ounces (Moz)	Tonnes (Mt)	Grade (g/t Au)	Ounces (Moz)	Tonnes (Mt)	Grade (g/t Au)	Ounces (Moz)
-	-	-	32.0	1.25	1.28	32.0	1.25	1.28

Notes:

1. *Ore Reserves are a subset of Mineral Resources.*
2. *Ore Reserves conform with and use the JORC Code 2012 definitions.*
3. *Ore Reserves are calculated using a gold price of A$2,200/oz.*
4. *Ore Reserves are calculated using a cut-off grade of 0.60 g/t Au.*
5. *All figures are rounded to reflect appropriate levels of confidence which may result in apparent errors of summation.*

4.4 Metallurgy

Metallurgical testwork samples were collected from diamond drilling completed in November 2021 and selected diamond drill core recovered from earlier exploration drilling programs. Samples were selected from more than 1,700 intervals in 11 drill holes (a mass of some 2,090 kg) and delivered to a metallurgical testing laboratory (ALS Laboratories) in Perth.

The testwork flowsheet was compiled by the process engineers and reviewed by the consulting metallurgist before confirmation by the laboratory. Diamond drill core of transitional and fresh rock was used to create five composites of the ore zones for metallurgical testwork. An additional nine fresh/transitional composites and three oxide composites were tested for variability.

Initial testwork program included:

- comminution tests to estimate work indices, material strengths and densities
- head assays
- gravity and leach testwork
- leach optimisations
- reagent optimisations
- thickening and process engineering testing.

Testing was completed on the five main composites to optimise the recoveries and reagent additions. Optimised recovery and reagent consumption conditions were replicated for the variability samples to determine orebody variability, and confirm the oxide zone recovery and reagent consumptions (as the oxide will contribute to the ore blend). The testwork included resource area material considered for the PFS mill feed, providing a basis for engineering parameters to design the proposed processing plant, and economic evaluation.

4.5 Processing plant

Ausgold engaged GR Engineering Services Limited (GRES) to develop the PFS processing plant design and associated cost estimates. The processing plant will treat a blend of oxide, transitional and fresh gold-bearing ores from the open pits at the KPG and is designed to operate at a throughput capacity of 3 Mt/a. The processing plant flowsheet was based on the results of metallurgical testwork and process calculations, estimations and assumptions using the following unit processes:

- primary crushing
- ore bin
- comminution, including semi-autogenous grind (SAG) milling, ball milling and pebble crushing (SABC) circuits
- gravity gold recovery
- pre-leach thickening
- carbon-in-leach (CIL) circuit
- elution and gold recovery
- tailings disposal.

The process flowsheet is shown in Figure 13.

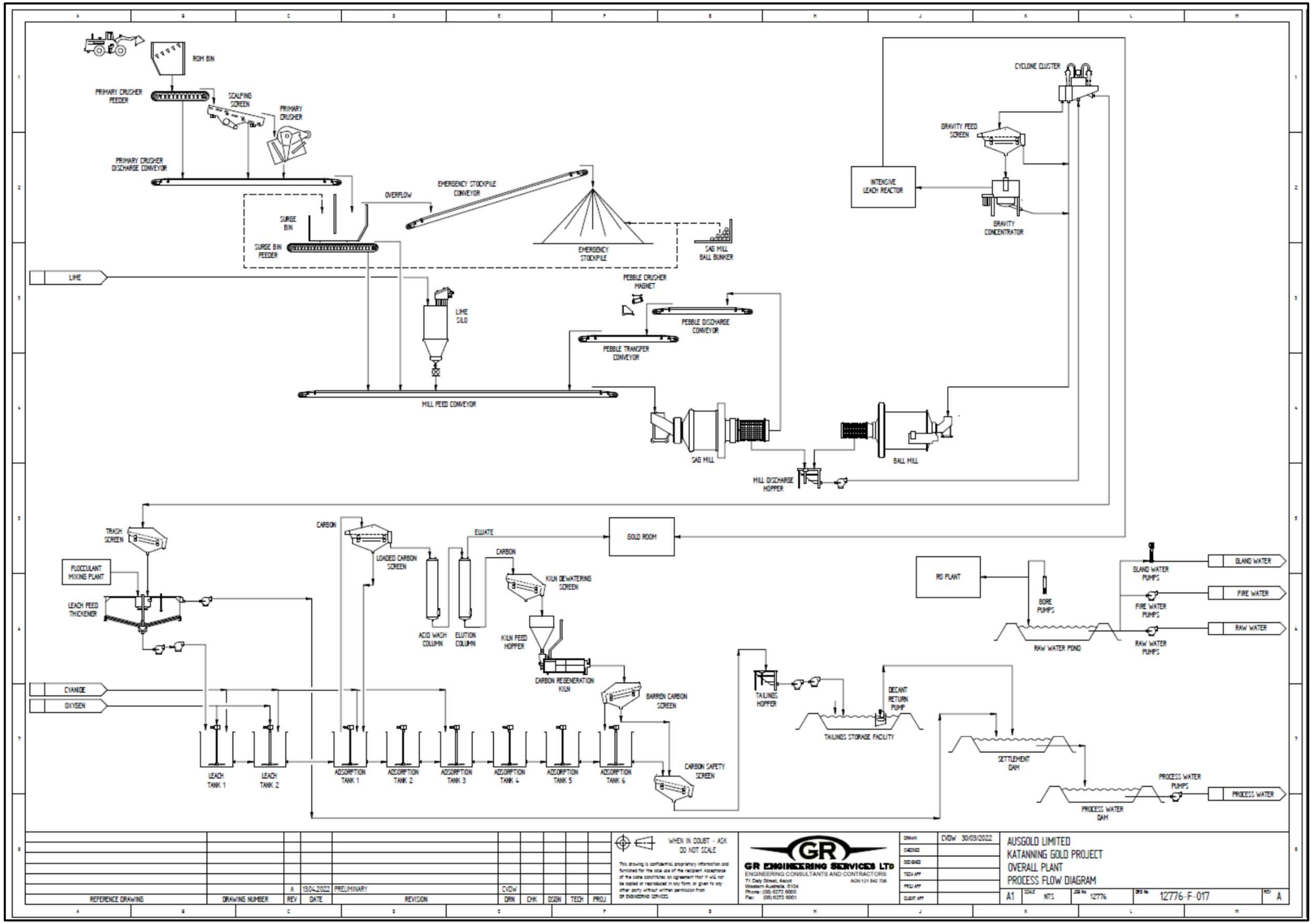

Figure 13: Process flowsheet

The surface mining ore will be hauled direct from the open pits and dumped in ore fingers on the run-of-mine (ROM) pad. Ore stockpiled on the ROM pad will be reclaimed, based on blending requirements, by front end loader and delivered to the crusher feed bin.

The crushing circuit will be a conventional open circuit jaw crusher. Product from the crushing circuit will be conveyed to a surge bin with an overflow emergency stockpile. The crushed ore will be transported by conveyor to the surge bin.

An emergency reclaim feeder fitted with a variable speed drive will be provided as means to recover ore from the emergency stockpile. Quicklime will be added onto the mill feed conveyor to provide protective alkalinity in the CIL circuit.

The mill feed conveyor will feed the SABC (SAG mill, ball mill and recycle crushing) comminution circuit. The first stage will be a grate discharge SAG mill in open circuit with pebble crushing and the second stage will be an overflow discharge ball mill in closed circuit with cyclones. The processing plant will operate at a nominal treatment rate of 375 dt/h and reduce the ore to a product size P_{80} of 75 µm. The grinding circuit utilisation will be 91.3%.

The SAG mill will have an 8.5 m diameter (inside shell) and 4.3 m effective grinding length. It will be a grate discharge, pinion drive mill fitted with a variable speed 6,000 kW motor. The SAG mill will be charged with 120 mm grinding media and designed to operate with a 15% ball charge. Slurry discharging from the SAG mill will be screened, with screen oversize being conveyed to a pebble crushing circuit. The pebble crushing circuit will include a single HP300 short head cone crusher. Pebble crusher product will be returned to the mill feed conveyor and recycled to the SAG mill.

The SAG mill’s variable speed drive will operationally compensate for changes in ore hardness. The design allows power consumption to be optimised for variations in the feed blend, assists in protecting the SAG mill liners from damage as a result of grinding media impact and minimises the mill motor current requirements on start-up. The variable speed drive will be configured to be used in the start-up for the ball mill, and once full rotational speed is achieved, the ball mill will be switched to direct online power. The variable speed drive will then be used to start and operate the SAG mill.

The combined SAG mill discharge screen undersize slurry and the ball mill discharge slurry will be pumped to a cyclone cluster for classification. The cyclone cluster will consist of 15 cyclones (each having a 400 mm diameter) – nine duty cyclones and six standby cyclones. Cyclone overflow will gravitate to the trash screens. Cyclone underflow will be split between the ball mill and the gravity circuit.

The ball mill will have a 6.4 m diameter (inside shell) and 9.6 m effective grinding length. It will be an overflow discharge, pinion drive mill fitted with a 7,000 kW motor. The ball mill will be designed to operate with a 30% ball charge.

The gravity circuit will consist of one centrifugal concentrator treating a portion of the cyclone underflow. Gravity concentrate will be intensively leached in a vendor-supplied reactor to yield a pregnant solution from which precious metals will be recovered in a dedicated electrowinning cell.

The classifier overflow from the grinding circuit will be screened to remove trash oversize. The screen undersize will be thickened to 50% solids and then leached using cyanide in a CIL circuit.

The CIL circuit will consist of eight 1,700 m^3 agitated tanks (two leach and six adsorption tanks) with a total nominal pulp residence time of 34 hours.

Cyanide will be stage dosed into the first two tanks and other CIL tanks as required. Oxygen will be injected into the CIL feed slurry pipe, through a Hyperjet pump installed on the first leach tank, and through sparge pipes in the CIL tanks.

Each CIL tank will have single, 12 m^2 mechanically wiped intertank screen to retain carbon. Carbon will be advanced on a batch basis through the CIL circuit counter-current to the pulp flow using recessed impeller pumps. Loaded carbon from the first stage of the CIL circuit will be pumped to the loaded carbon screen and screened carbon will then gravitate into the acid wash column of the elution circuit.

Carbon elution will be conducted using a split AARL elution circuit. Carbon recovered from the CIL safety screen will be acid washed and then stripped in separate 10-tonne capacity acid wash and elution columns. Stripped barren carbon will pass to the regeneration kiln and recirculated to the last tank in the CIL circuit. The design carbon advance rate for the circuit will be 6 t/d and six strips per week, based on a head grade of 1.3 g/t Au. The required carbon advance rate will be 6 t/d and the stripping frequency will be six elutions per week.

Pregnant solution from elution will be pumped to electrowinning cells in the gold room and the gold precipitated onto the stainless-steel cathodes. The electrowinning cells will be periodically cleaned and the resultant sludge filtered, dried and smelted to produce doré bars.

Final tailings from the CIL circuit will be screened to recover carbon fines and will then be pumped to the tailings storage facility (TSF) by a single-stage pumping system. Decant from the TSF will be returned to the settlement pond before overflowing to the process water pond.

Raw water will be sourced from boreholes located near the processing plant. The water will be pumped to the raw water tank at the processing plant via a system of overland pipelines and transfer pumps.

The raw water tank will supply water for the reverse osmosis plant and the gland sealing water pumps. The excess raw water will overflow to the raw water pond and supply the process facility requirements for raw water and fire water. The raw water pond will overflow to a lined 10,000 m^3 capacity process water pond. Thickener overflow will flow to a lined settlement pond and overflow will flow to the process water dam. Process water pumps will draw from the base of the process water pond to feed process water to the processing plant.

The processing plant control system will use programmable logic controllers (PLCs). The human machine interface (HMI) will use standard personal computers running Citect software to provide control. The main control room will be located in the grinding area with a subsidiary control room in the crushing area. Raw water abstraction from the borefields will be controlled and monitored from the main control room.

4.6 Tailing storage facility

Ausgold engaged Knight Piésold Pty Ltd to develop the PFS tailings storage facility (TSF) design and associated cost estimates. Knight Piésold determined that the TSF will be a paddock-style facility encircled by a zoned, downstream-constructed embankment and designed to store a total of approximately 30 Mt of tailings at an average deposition rate of approximately 3 Mt/a over 10 years. The total footprint area (including the basin area) will be approximately 220 ha.

The TSF will be initially developed as a single cell, with a second cell developed when Cell 1 nears the Stage 1 capacity. The initial storage capacity for Stage 1 will be 4.5 Mt, approximately 18 months of production, deferring construction timing of Stage 2 beyond the first 12 months of operation.

The embankments will be constructed in stages. The core zones will be constructed by a specialist earthworks contractor and the structural embankment will be constructed by the mining fleet as part of the mine waste operations from the open pits.

The design incorporates a composite lining system of compacted clay subgrade, partial basin HDPE liner and an underdrainage system. The design includes an underdrainage system and upstream toe drains at the embankments to reduce seepage losses and increase the water recycle to the processing plant.

Tailings will be discharged into the facility from the embankments by subaerial deposition methods, using banks of spigots at regular intervals to maintain the supernatant pond near the decant location. The decant system will pump supernatant water and collected rainwater to the processing plant via a decant return pipeline over the life of the facility. The active tailings beach will be regularly rotated around the facility to optimise tailings density.

Monitoring to identify any potential problems during operations will include:

- survey pins to check embankment movements
- piezometers along the embankment to measure the phreatic surface in the embankment and assess overall stability
- monitoring bores downstream of all embankments to measure groundwater levels and water quality.

The piezometers and bores will be measured monthly for water levels, electrical conductivity, pH and temperature, and quarterly for water quality.

4.7 Supporting infrastructure

The supporting infrastructure component (processing plant and mining surface infrastructure) includes:

- borefield pumps and piping to the plant site raw water pond
- power reticulation across the site
- overall project communications system

- pumps, piping, generator sets, tanks and reverse osmosis plant to produce and store potable water for the plant and mine service area (MSA)
- steel-framed and transportable buildings
- surface reticulation piping
- construction water supply, including pumping, piping, storage, treatment, and power generation
- site fencing and security
- processing plant security
- sewage facilities.

4.7.1 Power generation and reticulation

The PFS evaluated two options: independent power production (IPP) through a build-own-operate (BOO) contract, and connection to the Western Power grid with a supply contract through Synergy.

The IPP option involves a power generation mix of gas-fired generators, a solar photovoltaic array and battery storage, providing more than 25% of renewable energy penetration. Liquified natural gas (LNG) would be delivered daily and stored on site.

For the second option, existing power lines (currently servicing the site) would be upgraded to support the operations, connecting the site to the Katanning electrical substation. The overhead high voltage (HV) power lines from Katanning would be constructed and owned by Western Power and a supply contract with Synergy would be entered into. As part of the PFS, Western Power confirmed that it is technically viable to extend HV power lines to the site, following a planned upgrade of electrical switchgear and transformers at the Katanning substation, and Synergy provided a unit power cost quotation based on the estimated annual power demand. Furthermore, more than 20% of the power mix currently contributing to the grid is generated by renewable energy sources. With coal-burning power plants scheduled to be shut prior to 2030, it is estimated that more than 60% of the grid's power mix may be delivered through renewables.

For these reasons, it is envisaged that power for the site will be supplied from the grid. A substation will be constructed on site and power will be distributed to the various areas of the processing plant and supporting infrastructure via overhead power lines.

4.7.2 Water supply and treatment

The KGP will require installation of groundwater production bores for pit dewatering and raw water supply (i.e., as process water, dust suppression and potable water).

The number and depth of pit dewatering bores and bores required for raw water supply will be determined in the next phase of study. It is envisaged that all water abstracted from the pit dewatering bores will be directed to the raw water pond at the processing plant and additional make-up water will be sourced from dedicated bores.

Raw water will be treated on site through a reverse osmosis plant to supply potable water to the processing plant, offices and the MSA.

All bores and transfer pumps will be powered by generator sets or low voltage overhead power lines.

An organic wastewater treatment system will be installed to process all wastewater streams. This will be a 7.5 m^3/d capacity sewage plant to treat waste from the plant site facilities, offices and MSA.

4.7.3 Access roads

The site is accessible from Katanning via the Warren Road and Wolyaming Road, and the Katanning-Nyabing Road and Badgebup Road North. Ausgold's proposed infrastructure works do not include the upgrade or maintenance of these Katanning Shire roads. As the mining areas extend in the future, some roads may be truncated by mining infrastructure and will require re-alignment.

Non-mining roads in the site area include:

- MSA access road
- TSF access road
- magazine access road
- borefield access road.

All roads will be upgraded to a fit-for-purpose status.

4.7.4 Accommodation

The proximity to Katanning and other neighbouring villages provides opportunities to accommodate construction staff and the operation's personnel locally, which has a flow-on positive effect on local businesses. During construction, personnel will be accommodated in a mixture of locations and it is reasonable to assume that:

- Most of the personnel, particularly earthworks personnel, will be sourced from within the area, and will not require accommodation.
- Supervisors and managers will be accommodated in rented homes in Katanning and surrounding area.
- Overflow personnel will be accommodated in hotels within the region.

The PFS also identified an opportunity to renovate an existing facility in Katanning that would be well suited to accommodate personnel during construction and operations. The existing facility includes a dining area, commercial kitchen and laundry, administration office, ablutions and recreation facilities. The facility will require renovation to make it suitable as hotel-style accommodation, and a renovation cost estimate was added to the project's capital cost.

It is envisaged that all permanent staff will be accommodated in Katanning or neighbouring communities.

4.7.5 Plant area buildings

A processing plant office, with individual offices, an open-plan area, and a meeting room, will be constructed for technical personnel. Other buildings will include a first aid office and treatment room, plant crib room, ablutions, stores office and a workshop office.

Other buildings constructed at the processing plant site will include:

- a processing plant workshop and warehouse
- a light vehicle wash-down bay and sump adjacent to the processing plant workshop
- a reagent storage building
- a steel-framed building for the gold room
- a wet analytical laboratory and sample preparation building.

4.7.6 Administration office

The administration office will be established in Katanning for use by the General Manager, human resources, community relations, accounting and environmental management personnel.

4.7.7 Project construction office

The existing exploration office building at the site will be converted into a project construction office at the commencement of project execution. The current office building comprises offices, an open-plan area and a meeting room. An ablution block is offset from the office building and a kitchen building is also in place, complete with rooms available for storage or additional offices.

4.7.8 MSA offices and workshop

The MSA offices will share services with the processing plant's office and workshops.

The MSA office complex will include a mining office for personnel and contractor supervision, crib room and ablutions.

The MSA will include workshops for servicing the surface mining fleet, including heavy vehicles and ore haulage vehicles. It is assumed light vehicles will be serviced in Katanning. A transportable building for maintenance supervision will be attached to the workshop. Other facilities will include a fuel storage and re-fuelling facility and a wash-down bay suitable for both light and heavy vehicles.

4.8 Environment and community

The KGP lies in the southern part of the Wheatbelt region, in an area which has been almost entirely cleared for agricultural activities. The proposed project lies within the Avon Botanical District (https://www.anbg.gov.au/cpbr/anhsir/anhsir-manual/botanical-districts.html).

Several biological and heritage studies have been undertaken to support the approvals process for the KGP. These studies were commissioned to support exploration activities and provide baseline data, but have since expanded to support approvals for the development of the operation.

Ausgold proposes to undertake a self-assessment for the KGP to determine whether the project needs to be assessed under the *Environment Protection and Biodiversity Conservation Act 1999* (EPBC Act). If assessment is required, it is likely that assessment can be undertaken as an accredited assessment by the Western Australian Environmental Protection Authority (EPA) under the bilateral agreement. Ausgold therefore proposes to submit the EPBC Act referral and *Environmental Protection Act 1986* (EP Act) referral in parallel.

A summary of the environmental approvals schedule is included as Figure 14. Ausgold has reasonable grounds to expect that all necessary approvals and contracts will eventuate within the anticipated timeframe required by the mine plan.

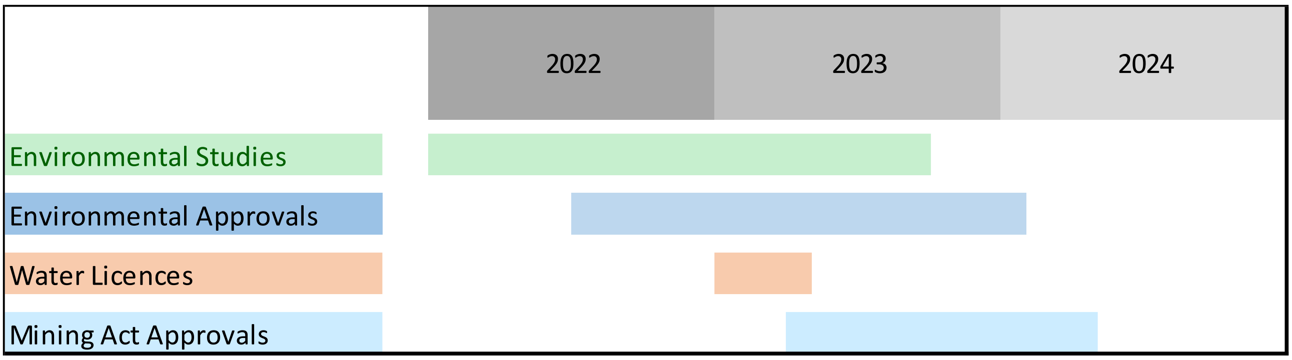

Figure 14: Environmental approvals schedule

Notes: Part IV requires referral of an Environmental Impact Assessment and is assessed by the Environmental Protection Authority (EPA). Part V requires submission of a Mining Proposal and is assessed by the Department of Mines, Industry Regulation and Safety (DMIRS).

The land area for the KGP is wholly situated within determined Native Title claims by the Noongar People and the Wagyl Kaip Traditional Owners have granted consent for Ausgold to use the area.

Ausgold commenced materials characterisation testwork on materials planned to be mined from the KGP. The waste characterisation programs will be developed in accordance with *Draft Guidance: Materials characterisation baseline data requirements for Mining Proposals* (DMP, 2016).

The KPG area lies within the Yilgarn South-West hydrogeological province. Ausgold will commission development of a preliminary water balance, undertake a water supply options assessment to identify likely sources of water and complete studies to meet approvals required to access those sources.

Ausgold is committed to maintaining good public relations through communication, consultation and engagement with key stakeholders and interested parties. Ausgold recognises the impacts and opportunities of its business and is confident it has the capabilities to achieve its environmental, social and governance (ESG) objectives.

Ausgold welcomes the initiatives outlined in the Western Australian Government’s Energy Policy WA, which provides a pathway for Ausgold to optimise efficiencies, adopt sustainable technologies and establish targets to benchmark emissions per ounce of gold produced.

4.9 Project capital and operating costs

4.9.1 Capital costs

The capital cost estimate is for the processing and engineering design, procurement and construction of a 3 Mt/a capacity processing plant and supporting infrastructure. The estimate is based on preliminary engineering, quantity take-offs, budget price quotations for major equipment and current cost data for similar activities and equipment. The estimate is quoted in Q2 2022 Australian dollars. The process and engineering designs were developed in sufficient detail to support capital and operating estimates to an accuracy of ±30%.

The capital estimate is based on the following:

- design, supply, construction, and commissioning of a 3 Mt/a processing plant (all costs reflect the purchase of new equipment)
- supply and construction of the processing plant offices, workshop, reagent store and warehouse
- an analytical laboratory and a sample preparation laboratory complete with equipment
- construction of the Cell 1 embankment of the paddock-style TSF
- pumping equipment and pipelines to supply raw water from a borehole supply area to the plant area
- establishment of the processing plant office, first aid facilities, stores and workshop
- establishment of the MSA complete with offices, crib room, ablutions, workshop, fuel storage and vehicle wash-down bay
- temporary power supplies for construction facilities prior to completion of the grid connection
- mobile equipment for surface mining, processing plant and administration
- supply of first fill items and capital spares
- engineering cost for design
- supervision and construction management
- temporary facilities required to undertake the project works
- owner's team cost and pre-production operating costs
- development of non-process infrastructure.

The overall capital cost estimate for the processing facility, supporting plant infrastructure and other surface infrastructure, and pre-production costs is **A$225.1 million**, inclusive of contingency. The cost estimate was developed in the second quarter (Q2) of 2022 to a +/-30% (PFS) level of accuracy and is summarised by area in Table 3.

Table 3: PFS capital cost estimate summary (at Q2 2022, +/- 30%)

Cost centre	Cost (A$ million)
Earthworks and roads	1.3
Plant capital	85.4
Tailings storage facility	12.8
Other site infrastructure	20.8
Project management and construction	31.9
Owner's project management team	4.4
First fills and spare parts	7.3
Indirect costs	7.6
Mining capital costs	5.6
Pre-production mining operating costs	41.0
Other pre-production operating costs	7.0
Total (including contingency)	**225.1**

Note: Figures are rounded to the nearest $A100k and rounding errors may be incurred.

4.9.2 Operating costs

The estimation of operating costs for the processing plant was based on the proposed processing plant feed ore schedule. No mining schedule was available at the time of providing the operating cost estimate, and allowance for change in the plant feed over this time has not been included.

The operating cost estimate for the processing plant at full production with transitional/fresh ore is A$51.9 million per year, equivalent to A$17.31 per tonne of ore treated; oxide ore may be treated at double the rate of the transitional/fresh ore, equating to a cost of A$14.02 per tonne. The processing costs by cost centre and ore types are shown in Table 4.

Table 4: PFS processing cost estimates by ore type

Cost centre	Transitional/Fresh (A$/t)	Oxide (A$/t)
Power	5.09	2.55
Maintenance spares & consumables	1.00	0.50
Operating consumables	8.02	9.38
Labour	2.53	1.26
General and administration	0.68	0.34
Total	**17.31**	**14.02**

The LOM mining cost, including labour, equipment, fuel, and mining general and administration (G&A), equates to A$28.48 per tonne of ore feed to the plant. The owner's G&A cost over the LOM, including (but not limited to) labour, vehicles, accommodation and office expenses, equates to A$3.72 per tonne of ore feed to the plant.

4.10 Project implementation

The contracting strategy for the processing plant is based on the principle that the responsibility for risk best resides with the party controlling and managing those risks. It is therefore envisaged that an experienced and competent contractor will be engaged to design and construct the processing plant on an engineering-procurement-construction management (EPCM) basis, providing cost effectiveness and a reasonable distribution of risk between the contractor and Ausgold, whereby Ausgold controls contingency. The EPCM contractor will act on behalf of Ausgold to develop the project and will guarantee the performance of the processing facility. The cost and schedule contingencies will be controlled by Ausgold.

On behalf of Ausgold, the EPCM contractor will manage all infrastructure, contractor and subcontractor requirements, and present progress claims for payment directly by Ausgold. While the risk and contingency for these major project infrastructure contracts ultimately remains with Ausgold, the arrangement will allow Ausgold to use a small owner's team.

The overall schedule duration is approximately 73 weeks from project approval to practical completion. Plant commissioning will commence on practical completion.

The schedule was developed based on the assumption that all equipment and materials will be new, and the contractor will have unhindered access to site. The implementation schedule encompasses the whole of the project works, including the processing facility and infrastructure.

An early commitment to critical path items is proposed. This enables procurement or design work for the following long-lead and critical items to be commenced (this must begin before regulatory approval to proceed is given):

- project definition documents
- processing plant and infrastructure layouts
- bulk earthworks, civil, mechanical, structural piping and electrical design
- long-lead equipment, including the primary crusher, SAG and ball mills, thickeners and CIL agitators.

4.11 Financial analysis

4.11.1 Methodology and inputs

Ausgold retained Northshore Capital Advisors Pty Ltd to create a cashflow model to evaluate, on a pre-tax and post-tax basis, the LOM plan and physical schedule provided by Resolve Mining Solutions, using cost inputs provided by Ausgold and other technical consultants to the project.

The objective of the financial model is to provide insight in regards to project value, the capital requirements to develop the project and the risk-to-reward associated with variability of cashflows.

The financial model is constructed on a quarterly basis in Australian dollars and is based on cost inputs as at Q2 2022.

The Company completed the PFS using a A$2,300/oz Australian dollar gold price as the gold price has remained above this level for the past 12 months and this price is currently A$175/oz less than the current spot price.

Prices and costs in the financial model are applied without escalation.

Corporate taxation is calculated by applying a 30% tax rate to taxable income after applying depreciation and adjusting for applicable tax losses. In this context, available tax losses at the end of 2023 financial year are estimated to be A$95 million, which assumes that Ausgold continues to satisfy the Continuity of Ownership test under the Division 165 of the *Income Tax Assessment Act*.

The financial model also considers adjustments for movements in working capital and GST.

4.11.2 PFS Base case financial outcomes

The PFS base case considers a 3 Mt/a gravity and CIL processing operation over 11 years, following a 1.5-year project construction period. The project processes 32.1 Mt of ore at 1.25 g/t Au, producing 1.16 Moz over LOM at an average of 105 koz per annum and a recovery of 90.4%. Over the first six years, higher grade ore at 1.47 g/t Au is processed, producing 758 koz at an average rate of 126 koz per annum. Project physicals are shown in Table 5.

Table 5: Project physicals

Description	Unit	LOM	To Production Year 6
Open pit ore mined	Mt	32.0	21.2
Waste mined	Mt	289.1	190.3
Ore & waste mined	Mt	321.1	211.5
Strip ratio	-	9.0 x	9.0 x
Gold grade mined	g/t	1.25	1.34
Gold contained in ore mined	Moz	1.3	0.9
Ore fed to processing plant	Mt	32.0	17.6
Gold grade fed (ROM grade)	g/t	1.25	1.47
Gold contained in ore feed	Moz	1.3	0.9
Gold recovered	Moz	1.2	0.8
Gold recovery	%	90.4%	90.9%

Note: Figures are rounded to the nearest $A100k and rounding errors may be incurred.

The KGP generates A$2.67 billion of revenue over the LOM, generating undiscounted cashflow after tax of A$540 million. The after-tax free cashflow generated during production is A$773 million. The financials clearly reflect the impact of significantly higher average gold production in the early years of the Project. Over the first six years of production, A$555 million of free cashflow after tax is generated at an average rate of A$92 million per annum, providing headroom and helping to de-risk the Project. Project cashflows are summarised in Table 6.

Table 6: Project cashflows

Description	LOM (A$ million)	To Production Year 6 (A$ million)
Gross revenue	2,669.1	1,744.2
Operating costs during production	(1,660.1)	(1,015.9)
Cash operating margin	1,008.9	728.3
Capital & operating costs during pre-production	(225.1)	(225.1)
Sustaining capital during production	(30.7)	(18.1)
Closure costs (incl. operating costs) after production	(7.6)	-
Movement in working capital	-	(12.9)
Undiscounted cashflow before tax	745.6	472.2
Tax payable	(205.3)	(142.6)
Undiscounted cashflow after tax	540.4	329.7
Free cashflow (after tax) generated during production	773.0	554.7

Note: Figures are rounded to the nearest $A100k and rounding errors may be incurred.

The strong cash generation over the early project years, combined with a pre-production capital and operating cost requirement of A$225 million, means that simple payback is achieved after only 21 months of production and the Project generates a 40.7% post-tax IRR. Post-tax project NPV (all equity) is A$364 million at a 5% discount rate. Selected financial metrics are summarised in Table 7.

Table 7: Financial metrics

Description	Value
Discount rate (Real)	5.0%
Project NPV (pre-tax)	A$514.8 million
Project NPV (post-tax)	A$364.2 million
Project IRR (pre-tax): Real	50.5%
Project IRR (post-tax): Real	40.7%
Pre-production capital and operating costs	A$225.1 million
Project payback period from production start (Real)	1.7 years

4.11.3 Cash costs

Project cash costs are calculated using the Brook Hunt methodology. The KGP demonstrates an all-in-sustaining cost (AISC) of A$1,481/oz over the LOM. The AISC (stockpile adjusted) for the first six years of production is A$ 1,370/oz. Favourable cash costs reflect the benefits of proximity to grid power and local services and labour. Cash cost components are shown in Table 8 and exclude A$8 million for closure costs.

Table 8: Project cash costs

	Description	LOM (A$ million)	Per ounce (A$/oz)
C1 Costs	Refining & doré transportation costs	5.8	5
	Third-party royalties	-	-
	Mining operating cost (during production)	912.6	786
	Stockpile adjustments (for pre-production ore mining)	27.9	24
	Processing operating cost	557.4	480
	General & Administration	119.2	103
	Subtotal - C1 Costs	**1,623.1**	**1,399**
C2 Costs	C1 Costs	1,623.1	1,399
	Initial Capital Depreciation	197.1	170
	Sustaining Capital Depreciation	30.7	26
	Subtotal - C2 Costs	**1,850.9**	**1,595**
C3 Costs	C2 Costs	1,850.9	1,595
	WA State Royalty	65.0	56
	Subtotal - C3 Costs	**1,915.9**	**1,651**
AISC	C3 Costs	1,915.9	1,651
	Initial Capital Depreciation	(197.1)	(170)
	All-in Sustaining Cost (AISC)	**1,718.7**	**1,481**

Note: Figures are rounded to the nearest $A100k and rounding errors may be incurred.

4.11.4 Sensitivity analysis

The PFS results demonstrate a robust economic case with a gold price of A$1,689/oz required to achieve NPV breakeven (inclusive of all initial, ongoing and closure capital and operating costs).

Sensitivity analysis was conducted on gold price and capital and operating costs in a range of +/-30% in increments of 10%, and after-tax NPV results for each parameter in turn were recorded. The analysis shows that the Project is most sensitive to gold price, around 60% to 65% as sensitive to operating costs and about 10% as sensitive to capital costs, as summarised in Table 9.

Table 9: Sensitivity analysis

Parameter	Sensitivity applied to generate after tax NPV below						
	(30.00%)	(20.00%)	(10.00%)	0%	10.00%	20.00%	30.00%
Gold price	(59.82)	92.8	228.9	364.2	498.8	633.4	767.9
Operating costs	620.37	535.0	449.6	364.2	278.3	191.9	105.3
Capital & sustaining capital	410.12	394.8	379.5	364.2	348.9	333.6	318.3

Note: Figures are rounded to the nearest $A100k and rounding errors may be incurred.

An evaluation of sensitivity to gold price was conducted in the range of A$2,000/oz to A$2,600/oz in increments of A$100/oz. The after-tax cashflow, NPV and IRR results are shown in Table 10.

Table 10: NPV and IRR sensitivity to gold price

Gold price	A$2,000/oz	A$2,100/oz	A$2,200/oz	A$2,300/oz	A$2,400/oz	A$2,500/oz	A$2,600/oz
Cashflow after tax	299.5	380.0	460.6	540.4	620.1	699.8	779.6
NPV_5 after tax	187.58	246.6	305.7	364.2	422.8	481.3	539.8
IRR after tax	25.7%	31.0%	36.0%	40.7%	45.3%	49.8%	54.2%

NPV_5 – NPV with 5% discount rate applied; figures are rounded to the nearest $A100k and rounding errors may be incurred.

An evaluation of sensitivity to discount rate was conducted in 1% increments between 5% of 10%. Sensitivity to increases in discount rate are countered by the upfront scheduling of higher-grade ore. The after-tax NPV results are shown in Table 11.

Table 11: NPV sensitivity to discount rate

Discount rate	5.00%	6.00%	7.00%	8.00%	9.00%	10.00%
NPV_5 after tax	364.2	337.1	312.1	289.0	267.6	247.8

Note: Figures are rounded to the nearest $A100k and rounding errors may be incurred.

4.11.5 Funding

The PFS estimates a funding requirement of A$225 million to cover the capital and operating costs from the start of plant construction to the end of plant commissioning and the start of gold production. It is expected that the funding requirement will be met with a mixture of debt and equity, which will need to be raised before project construction can begin. The KGP generates A$773 million of free cashflow after tax during production and A$555 million of free cashflow after tax during production over the first six operating years, suggesting that it will be amenable to project financing using a typical mix of debt and equity.

Additional funds will be required to progress the project through to final feasibility and financial investment decision. It is anticipated that the Company will be able to raise these funds via equity markets.

Appendix 2: JORC Code Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	The database that Ausgold has compiled for the KGP area contains over 4,062 drill holes, totalling over 234,137m of drilling comprising a variety of techniques, including diamond coring (DD), reverse circulation (RC), aircore (AC), and rotary air blast (RAB). Approximately 24% of the holes (14% of the metres) were drilled prior to Ausgold's involvement in 2011, and the derived information is hereafter referred to as historical data. Only RC and DD data were used for the preparation of the Dingo, Jinkas, Jackson, White Dam, Olympia and Datatine Resource estimates, equating to approximately 3,387 holes and 41,030 samples (totalling 41,180m) used directly for estimation after compositing to 2.5m. Only limited information is available for the historical programs, and the descriptions below primarily pertain to the Ausgold programs. The validity of the historical data has been assessed by local comparisons with the Ausgold data. **RC Drilling** Samples from RC drilling were collected in one metre intervals in mineralised zones with a 1/8 split for assay, split by a cyclone-mounted cone splitter or standalone splitter, bagged in pre-numbered calico bags and the remainder retained in large plastic bags. In non-mineralised zones, a spear sample was collected from each 1m interval and composited to 3m. Where composite samples returned assays at or above 0.5 g/t Au, the original 1m samples were riffle split and submitted for assaying. Each RC metre sampled weighed approximately 2 to 3 kg. The samples were sent to a range of Perth based laboratories (ALS, SGS, QAS, Ultratrace and Minanalytical) for sample preparation and assaying. For photon analysis from 2021 onwards (Minanalytical), samples were crushed to -3mm and split to produce a 500g sample for analysis (PAAU02). For fire assay analysis from 2013-2021, the samples were sorted, weighed, dried, crushed to -2mm in a jaw crusher then subsequently pulverised to achieve a nominal particle size of 85% passing <75µm to create 50g charges for analysis. Prior to 2013, analysis was via 40g aqua regia with an AAS finish. **DD Drilling** Samples were nominally collected at 1m intervals; however, where appropriate the geologist adjusted these intervals to match geological intervals. The samples were sent to Perth based laboratories (ALS, SGS, QAS and Ultratrace) for sample preparation and assaying. The samples were sorted, weighed, dried, crushed to -2mm in a jaw crusher then subsequently pulverised to achieve a nominal particle size of 85% passing <75µm to create 50g charges for fire assay analysis with an AAS finish. Prior to 2013, analysis was via 40g aqua regia with an AAS finish.

Criteria	JORC Code explanation	Commentary
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	The sample data used for resource estimation were derived from RC or diamond core drilling. **RC Drilling** The RC drill rigs were equipped with 139mm to 143mm diameter face-sampling bits. **DD Drilling** Diamond core drilling was conducted using HQ or NQ coring equipment (triple and standard tubes). Drill core was orientated at least every 3-6m.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/ coarse material.*	**RC Drilling** A semi-quantitative estimate of sample recovery was done for each sample. Drill sample recovery approximates to 100% in mineralised zones. Samples were typically collected dry, with variations from this recorded in the drill log. The cyclone-mounted cone splitter, or standalone splitter, was cleaned thoroughly between rod changes. The cyclone was cleaned every 30m, or between rod changes when the sample is wet. In addition, the cyclone was generally cleaned at the base of transported cover and the base of complete oxidation, and after each hole to minimise cross- hole contamination. **DD Drilling** A quantitative measure of sample recovery was done for each run of core. In completely and partially weathered zones core was drilled using the triple-tube method to maximise recovery. Recoveries were generally excellent (>90%), with reduced recovery in the initial near- surface sample and transported cover material. The relationship between sample recovery and grade and whether bias has been introduced has not been investigated at this stage.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.* • *The total length and percentage of the relevant intersections logged.*	All holes in the current program have been geologically logged to a high level of detail to support the definition of geological domains appropriate to support Mineral Resource estimation and classification. **RC Drilling** Representative rock chips from every metre were collected in chip trays and logged by the geologist at the drill site. Lithology, weathering (oxidation state), veining, mineralisation and alteration are recorded in detail using standard digital logging sheets and defined look-up tables to ensure that all data is collected consistently. Logging data is entered using tablet computers. All data is validated by the logging geologist before being entered in an AcQuire database.

Criteria	JORC Code explanation	Commentary
		All chip trays are photographed using a SLR camera and images recorded using the cloud-based Imago system. Historical chip trays are currently being re-photographed. **DD Drilling** Lithology, weathering (oxidation state), structure, veining, mineralisation and alteration are recorded in detail using standard digital logging sheets and defined look-up tables to ensure that all data is collected consistently. In addition, structural and geotechnical logging is also completed on diamond core. Logging data is entered using tablet computers. All data is validated by the logging geologist before being entered in an acQuire database. Geotechnical logging is not possible on RC samples. All core trays are photographed using a SLR camera and images recorded using the cloud-based Imago system. Historical core tray photographs are currently being uploaded to the imago system.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	**RC Drilling** RC samples were collected from each 1m interval from the rig mounted cone splitter or standalone splitter configured to give a 1/8 split. Field duplicates (additional split from RC) were collected at a frequency of 1 in 30 or 1 in 20 samples. QAQC samples consisting of certified standards and blanks were inserted in the sequence of assay samples at a frequency of 1 in 25 or 1 in 50 samples. The blanks were inserted as pulps during the initial drill programs and as both pulp and coarse blanks for subsequent programs. For photon assay analysis from 2021 onwards (Minanalytical), samples were crushed to -3mm and split to produce a 500g sample for analysis (PAAU02). For fire assay analysis from 2013-2021 (ALS, SGS, QAS and Ultratrace), samples were sorted, weighed, dried, crushed to -2mm in a jaw crusher then subsequently pulverised to achieve a nominal particle size of 85% passing <75µm to create 50g charges for fire assay with an AAS finish. Prior to 2013, analysis was via 40g aqua regia with an AAS finish. **DD Drilling** NQ or HQ drill core was split with a diamond bladed core saw, with half or quarter core sent for assay. Samples were nominally collected at 1m intervals; however, where appropriate the geologist adjusted these intervals to match geological intervals. QAQC samples consisting of certified standards and blanks were inserted into the sequence of assay samples at a rate of 1 in 25 or 1 in 50 samples. The blanks were inserted as pulps during the initial drill programs and as both pulp and coarse blanks for subsequent programs. At a range of Perth based laboratories (ALS, SGS, QAS and Ultratrace), samples were sorted, weighed, dried, crushed to -2mm in a jaw crusher then subsequently pulverised to achieve a nominal particle size of 85%

Criteria	JORC Code explanation	Commentary
		passing <75µm to create 50g charges for fire assay analysis with an AAS finish from 2013 onwards. Prior to 2013 analysis was via 40g aqua regia with an AAS finish. The Competent Persons consider that the sample weight and grind size combinations are considered appropriate for the oxide and fresh mineralisation at the KGP.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	**RC Drilling** Analysis for gold was via photon assay (PAAU02) for the 2021-2022 drill programs, by 50g fire assay with an AAS finish for the 2013-2021 drill programs and by 40g aqua regia with an AAS finish prior to 2013. Field quality control procedures adopted comprised of entering a sequence of matrix matched commercially certified reference materials (CRMs), and blanks into the sample run at a frequency of approximately 1 in 25 or 1 in 50 samples. Field duplicates were collected every 1 in 30 or 1 in 20 samples. Gold CRMs have been sourced from OREAS, Geostats Pty Ltd and Gannet Holdings, and are used to check accuracy and bias of the analytical method. Gold certified values have ranged between 0.32g/t and 7.07g/t. Blank material was sourced from Geostats Pty Ltd and should be below detection limits. Certified reference materials are used to check accuracy and bias of the analytical method. The results were similar to the standard concentration for the specific standard. QAQC samples were monitored on a batch-by-batch basis. An assay batch is accepted if the blank samples are within the acceptable limits (5 times the lower detection limit) and the standards are within the + 3SD (standard deviations). One failed standard can cause rejection if the results around the failed standard are not in the normal grade range. A batch is also re-assayed when assay results from two or more standards are outside the acceptable limits. The inserted blank materials did not show any consistent issues with sample contamination. Review of CRMs and blanks suggest that an acceptable level of accuracy (lack of bias) has been established. The performance of field duplicates in RC samples is generally reasonable and the variations are related to the style of mineralisation. Internal laboratory checks are conducted including insertion of CRMS, blanks and conducting lab duplicates. Review of the internal laboratory QAQC checks suggests the laboratory is performing within acceptable limits. **DD Drilling** Analysis for gold was via 40g aqua regia with an AAS finish prior to 2013 and by 50g fire assay with an AAS finish after 2013.

Criteria	JORC Code explanation	Commentary
		Field quality control procedures adopted comprised of entering a sequence of matrix matched commercially certified reference materials (CRMs), and blanks into the sample run at a frequency of approximately 1 in 25 or 1 in 50 samples. Gold CRMs have been sourced from OREAS, Geostats Pty Ltd and Gannet Holdings, and are used to check accuracy and bias of the analytical method. Gold certified values have ranged between 0.32g/t and 7.07g/t. Blank material was sourced from Geostats Pty Ltd and should be below detection limits. Certified reference materials are used to check accuracy and bias of the analytical method. The results were similar to the standard concentration for the specific standard. QAQC samples were monitored on a batch-by-batch basis. An assay batch is accepted if the blank samples are within the acceptable limits (5 times the lower detection limit) and the standards are within the + 3SD (standard deviations). One failed standard can cause rejection if the results around the failed standard are not in the normal grade range. A batch is also re-assayed when assay results from two or more standards are outside the acceptable limits. The inserted blank materials did not show any consistent issues with sample contamination. Review of CRMs and blanks suggest that an acceptable level of accuracy (lack of bias) has been established. Internal laboratory checks are conducted, including insertion of CRMs, blanks and conducting lab duplicates. Review of the internal laboratory QA/QC checks suggests the laboratory is performing within acceptable limits.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	High standard QAQC procedures are in place, therefore repeatability issues from a QAQC point of view are not considered to be significant. Significant and/or unexpected intersections were reviewed by alternate company personnel through review of geological logging data, physical examination of remaining samples and review of digital geological interpretations. All assay data was accepted into the database as supplied by the laboratory. Data importation into the database is documented through standard operating procedures and is guided by AcQuire import validations to prevent incorrect data capture/importation. Geological, structural and density determination data is directly captured in the database through a validation-controlled interface using Toughbook computers and AcQuire database import validations. Primary data is stored in its source electronic form. Assay data is retained in both the original certificate (.pdf) form and the text files received from the laboratory. Data entry, validation and storage are discussed in the section on database integrity below.

Criteria	JORC Code explanation	Commentary
		The database contains a number of RC and diamond core holes that are sufficiently close to be used to prepare twinned datasets. Twinned data comparisons indicated similar characteristics in terms of grade tenor and intercept thicknesses, with generally no significant issues identified. No adjustments to assay data were undertaken.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	Drill holes are reported in MGA94 datum, UTM zone 50 coordinates. Elevation values were in AHD. Drill hole collars (and drilling foresight/backsight pegs) were set out and picked up using a differential GPS, which provided +/- 100 millimetre accuracy. For Ausgold drill holes, an end of hole gyroscopic drill hole survey was completed by the drilling contractors using a Reflex EZ tool or an Axis Mining Camp Gyro tool. The gyro measured the first shot at 0m followed by every 10m down-hole. The data was examined and validated onsite by the supervising geologist. Any surveys that were spurious were re-taken. Historical drill holes were variably downhole surveyed at 20-30m intervals. Validated surveys were entered into the AcQuire data base.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Dingo: Drill spacing is typically 20-40m along 20-40m spaced section lines. Most holes are angled at 60° towards 244°. In the southern part of the deposit, drill spacing is typically 50m along 50m spaced section lines, with most holes angled at 60° towards 270°. • Jinkas: Drill spacing is typically 10-20m along 20m spaced section lines through the central and north-western parts of the deposit. In the south-eastern part of the deposit drill spacing is approximately 40-60m along 100m spaced section lines. Most holes are angled at 60° towards 244°. • Jackson: Drill spacing is variable and ranges from 20-60m along 30m-120m spaced section lines. The dataset comprises a mix of shallow vertical holes (mainly in the southern half and on the western side of the deposit), and deeper holes are typically angled at 60° towards 244°. • White Dam: Drill spacing is variable and ranges from 20-40m along 20-100m spaced section lines. The dataset comprises a mix of shallow vertical holes (mainly on the western side of the deposit), and deeper holes are typically angled at 60° towards 244°. • Olympia: Drill spacing is variable and ranges from 30-100m along 20-100m spaced section lines. Most holes are angled at 60° towards 244°. • Datatine: Drill spacing is variable and ranges from 20-60m along 40-80m spaced section lines. Drill holes are typically angled at 60° towards 335°. At these drill spacings, the lodes can be clearly traced between drill holes. The variography indicated practical grade continuity ranges of approximately 30-60m.

Criteria	*JORC Code explanation*	Commentary
		Over 90% of the data used for resource estimation were derived from samples collected on 1m intervals, with most of the remainder derived from smaller intervals. The datasets were composited to 1m intervals prior to grade estimation.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	The orientation of the mineralised lodes is quite consistent over the project area. Most of the drill holes are oriented orthogonal to the regional strike, and with a declination of 60°. This results in an approximate right angle intersection with the lodes, which typically dip at between 30° - 45° parallel to the gneissic foliation.
Sample security	• *The measures taken to ensure sample security.*	All drill samples were systematically numbered and placed in pre-printed (numbered) calico bags and placed into numbered polyweave bags which were tied securely and marked with flagging. Assay samples were stored at a dispatch area and dispatched weekly. Samples were shipped via Katanning Logistics directly to labs in Perth. The sample dispatches were accompanied by supporting documentation signed by the geologist and showing the sample submission number, analysis suite and number of samples. The chain of custody is maintained by the labs once the samples are received on site and a full audit is conducted. Assay results are emailed to the responsible geology administrators in Perth and are loaded into the AcQuire database through an automated process. QAQC on import is completed before the results are finalised.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	An independent review of the primary and quality assurance data was conducted by Snowden in 2011, SRK in 2019 and 2021, as well as by Snowden Optiro in December 2021 and May 2022. Ausgold conducted internal audits in 2013 and 2015. Before the commencement of the 2021-2022 RC and Diamond drilling programs, the sampling process was fully reviewed and documented as a standard company process. Several operational and technical adjustments were identified to improve validation of collected data, interpretation of data and management of QAQC practices. These improvements have been updated into standard operating procedures.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	The reported resources are all from 100% owned Ausgold Exploration Pty Ltd Mining Tenements (wholly owned subsidiary of Ausgold Limited), which include M70/210, M70/211, E70/2928 and M 70/488. Apart from reserved areas, the rights to surface land use are held under freehold titles. Ausgold has entered into access and compensation agreements with freehold landowners that permit exploration activities. The tenements are in good standing, and all work is conducted under specific approvals from the Department of Mines, Industry Regulation and Safety (DMIRS). Apart from reserved areas, rights to surface land use are held under freehold titles. Ausgold has entered into access and compensation agreements with freehold landowners that permit exploration activities. Written consent under section 18(3) for Jinkas Hill dated 24 January 2018 was granted by Honourable Ben Wyatt MLA to disturb and remove the registered Aboriginal Heritage Site 5353 known as "Jinkas Hill" which is located on the eastern side of the Jinkas Pit.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	Gold mineralisation was discovered by Otter Exploration NL in 1979 at Jinkas Hill, Dyliabing, Lone Tree and White Dam when investigating stream sediment anomalies. Between 1984 and 1988, Otter and related companies evaluated the region with several other explorers including South West Gold Mines and Minasco Resources Pty Ltd. In 1987, Glengarry Mining NL purchased the project and in 1990 entered into a joint venture with Uranerz who agreed on minimum payments over three years to earn 50% interest. Uranerz withdrew from the project in 1991 after a decision by their parent company in Germany to cease Australian operations. International Mineral Resources NL (IMR) purchased the mining leases and the Grants Patch treatment plant from Glengarry Mining NL in 1995 and commenced mining at the Jinkas deposit in December 1995. Ausgold understands the mine was closed in 1997 after producing approximately 20,000 oz of gold from the Jinkas and Dingo Hill open cuts at a head grade of approximately 2.4 g/t. It is understood that mine closure was brought about by a combination of the low gold price of the time (<US$400/oz) and the inability of the processing plant's comminution circuit to process hard ore from below the base of weathering. Reports from the period indicate that the ore bodies were reasonably predictable in terms of grade and continuity and appeared to produce consistent and reproducible results from grade control. (Ravensgate, 1999). Great Southern Resources Pty Ltd (GSR) purchased the mining and exploration leases from IMR in August 2000.

Criteria	JORC Code explanation	Commentary
		Ausgold entered into a joint venture with GSR in August 2010, and the mineral titles were transferred to Ausgold in entirety in August 2011.
Geology	• *Deposit type, geological setting and style of mineralisation.*	The project includes 2 main deposit areas, comprising Jinkas in the north, and Dingo in the south. The Jinkas area is subdivided into a set of named mineralised zones including Jinkas Hangingwall, Jinkas Footwall-White Dam, Jackson, and Olympia lodes. The majority of the project area is overlain by residual clays, with outcrop mostly limited to remnants of lateritic duricrust on topographic highs. Gold mineralisation is hosted by medium to coarse-grained mafic gneisses, which dip at around 30° - 45° towards grid east (68°). These units represent Archaean greenstones metamorphosed to granulite facies. The mineralised gneissic units are interlayered with barren quartz-monzonite sills up to approximately 120 m thick and are cross-cut by several Proterozoic dolerite dykes that post-date mineralisation and granulite metamorphism. Gold predominantly occurs as free gold associated with disseminated pyrrhotite and magnetite, with lesser amounts of pyrite and chalcopyrite and traces of molybdenite. Thin remnant quartz veins are associated with higher grade zones.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	A total of 230 Reverse Circulation (RC) holes for 22,413m and 7 diamond drill holes for 864.54m have been completed since September 2021 and have been included in the Resource estimation. The results of this drilling have been reported in ASX Announcements on: Dingo (7/02/2022; 06/05/2022), Jinkas (25/02/2022; 04/04/2022; 06/05/2022), White Dam (25/02/2022; 04/04/2022; 06/05/2022), Jackson (25/02/2022; 04/04/2022; 06/05/2022) and Olympia (06/05/2022).
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the*	All reported RC and DD assays have been arithmetically length weighted. A nominal 0.3g/t Au lower cut- off is reported with internal waste intervals (i.e. <0.3 g/t) to not exceed the width of a 2m. All material exploration results have been reported in previous market releases. Higher grade intervals within larger intersections are reported as included intervals and noted in results tables. No top-cut grades have been applied when reporting exploration results.

Criteria	JORC Code explanation	Commentary
	procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	The geometry of any primary mineralisation is such that it trends N-S to NNW-SSE and dips moderately (30°-45°) to the east. Given this, drilling intersects mineralisation at a high-angle and downhole intercepts approximate true widths in most cases. If down hole length varies significantly from known true widths then appropriate notes are provided.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Refer to figures in previous market releases.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All results used have been reported in ASX announcements: Dingo (7/02/2022; 06/05/2022), Jinkas (25/02/2022; 04/04/2022; 06/05/2022), White Dam (25/02/2022; 04/04/2022; 06/05/2022), Jackson (25/02/2022; 04/04/2022; 06/05/2022) and Olympia (06/05/2022).
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	At this stage there are no substantive other exploration data from the recent drilling that is meaningful and material to report.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	As mineralisation is not closed off along strike and down dip of all interpreted lodes, further drilling will test extent of mineralisation.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	Resource data are stored in an AcQuire database, which is managed by a database administrator. All data loading was via electronic transfer from checked primary data sources. The import scripts contain sets of rules and validation routines to ensure that the data are of the correct format and within logical ranges. Extracts were checked to ensure the consistency of data across related tables. External and internal reviews of the database were conducted in 2011, 2013, 2015, 2017, 2020, 2021 and 2022.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	Site visits have been conducted by the Ausgold CP who takes responsibility for the geology model and data integrity. A site visit has been undertaken by the Resource Estimation CP (Dr Michael Cunningham of Sonny Consulting Services) on 3-4 November 2020. The CP inspected some rock chips, exposed geology from historic open pits, and observed drilling and sampling of the 2020 drill campaign. Drilling and sampling were undertaken in a professional manner with due diligence for QA/QC being adhered to.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	The geological interpretation is considered consistent with site observations and with the broadly accepted understanding of the regional geology by the mining community. Structural studies were performed to derive conceptual models of lode geometry and controls on mineralisation. Lode definition was primarily based on geochemical data, lithological and structural logs, with boundaries typically defined by distinct changes in gold grade and known regional folding. Lode geometry was observed to be relatively constant over the defined extents, and the interpreted models were consistent with the structural models. Waste was also modelled which includes a large intrusion of Quartz Monzonite occurring as a sill within a tight synformal structure with the Jinkas footwall on the upper limb and White Dam on the lower limb. The fold is cored by a large intrusion of quartz monzonite. Several post-mineralisation igneous dykes are also present and have been modelled from drillhole logs. In certain cases, the logged dykes had gold grades and this was checked and deemed to be an incorrect log. The dyke rock chip and mineralised gneiss rock chip can look very similar in places. The modelled igneous rocks provided useful markers for modelling the mineralised lodes. Where dykes cross the lodes, the volume from the wireframe was clipped.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	Twenty-six sub-parallel lodes were defined for Jinkas. White Dam consists of one folded lode structure, and two smaller White Dam sub parallel lodes. The Jinkas White Dam structure is folded around a shallowly (~35°dipping to the ENE) synformal axis. The lodes strike to the NNW and dip at approximately 35° to the ENE, and the fold has a shallow plunge

Criteria	JORC Code explanation	Commentary
		toward the northeast. They have defined strike lengths of 3,300 m, and dip extents ranging from 150 m to 480 m. The Jinkas Footwall – White Dam lode averages 3-5m on the limbs and thickens into the core of the fold up to 20m. The lodes have been interpreted to the surface and modelled to a depth of up to 420 m. Twenty-four sub-parallel lodes were defined for Olympia. The lodes are the northern extension of Jinkas and White Dam, but current drill hole coverage does not permit linking up at this stage. The lodes generally strike to the NNW and dip at approximately 25° to the ENE. They have a defined strike length of approximately 850 m and a dip extent of approximately 400m. The average lode thicknesses range from approximately 2 m to 6 m. Like Jinkas/White Dam, the lodes have been modelled around the major synform which is cored by the Quartz Monzonite intrusion. A total of thirty-two sub parallel lodes were defined for Jackson. The deposit is cross-cut by an east-west striking dyke, and to the northeast by another northwest-southeast striking dyke. All lodes have a sinistral offset by the major central dyke except the shallowest lode in the south, which is not present to the north. The Jackson lodes strike to the NNW and dip at approximately 30° to the ENE. They have defined strike lengths ranging from 150 to 5,000 m, and, and dip extents ranging from 285 m to 624 m. The Main and Hanging wall lode thicknesses average 5 m and the Footwall lode thickness averages 3m. The lodes have been interpreted to the surface and modelled to a depth of up to 500m. A total of 16 sub-parallel lodes were defined for Dingo-Rifle Range. The lodes strike to the NNW and dip at approximately 30° to the ENE. They have defined strike lengths ranging from 450 to 1,900m, and dip extents ranging from 220 to 420 m. The lode thicknesses average approximately 5 m. The lodes have been interpreted to the surface and to a depth of up to 250 m. Two dolerite dykes striking WNW truncate the mineralisation. Six sub-parallel lodes were defined for Datatine. The lodes strike to the NNW and dip at approximately 10° to the ENE. They have a defined strike length of approximately 400 m and varying dip extents of approximately 70-400m. The average lode thicknesses range from approximately 1 m to 2m. Mineral Resource reporting has been limited to a depth of approximately 160-180 m. The Datatine deposit is geologically distinctive from the other KGP gold mineralisation. Datatine is hosted within an altered pyroxenite, which dips at 45° towards the south. The change in orientation is accommodated by a regionally significant thrust fault along a NNE strike which separates the Datatine - Burong lode from the KGP to the south. For all deposits, geological lodes were modelled using 0.3 Au g/t wire frames and a cut-off grade of 0.6 g/t Au for Mineral Resource reporting has been limited to a depth of 150mRL, approximately 220 m below surface. Below 150mRL, a cut-off grade of 1.8 g/t Au is used to report an underground mineral resource estimate for Jinkas-White Dam.

Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	Samples were composited to 2.5m, with the assumption that the bench height of the future pit will be 2.5m. The resource estimates were prepared using conventional proportional block modelling and uniform conditioning techniques. Single models were prepared to represent the defined extents of the mineralisation for each deposit and include: 1) Jinkas / White Dam 2) Olympia, 3) Jackson / White Dam, and 4) Dingo The modelling of the lodes was completed using Micromine® and Vulcan®, and the Mineral Resource Estimates was performed using *Isatis .neo*®. KNA studies were used to assess a range of cell dimensions, and a parent estimation block size of 10 x 10 x 2.5 m (XYZ) was considered appropriate given the drill spacing, grade continuity characteristics, and the expected mining method. The nominal drill spacings range from 10 x 20 to 100 x 100m. In most cases, the lode wireframes were used as hard boundary estimation constraints. The drill data did not show evidence of significant supergene enrichment or grade trending with depth, and for this reason, the weathering surfaces were not used as estimation constraints. Probability plots and histograms were used to identify outlier values, with grade cuts applied accordingly. A summary of the top-cuts is presented below: *Jinkas / White Dam hangingwall top cut: 42 g/t Au* *Jackson / White Dam top-cut: 12 g/t Au* *Olympia top-cut: 6 g/t Au* *Dingo / Rifle Range top-cuts: 14 g/t Au* Further spatial distance restrictions, where appropriate, were applied to the high-grade samples. Additional distance restrictions of 15m were applied, where deemed appropriate, to limit the influence of high-grade outliers. In particular, where a high-grade cut was selected to minimise metal loss to no greater than 5% and where it was beyond the unbroken portion of a histogram tail, the grade at the tail was selected for distance restriction. For Olympia, Jackson and Dingo, the block grades were estimated using Uniform Conditioning (UC) on 10 by 10 by 2.5m panels. Search orientations and weighting factors were derived from variographic studies. A multiple-pass estimation strategy was invoked, with KNA used to assist with

Criteria	JORC Code explanation	Commentary
		the selection of search distances and sample number constraints. Extrapolation along strike and down dip was limited to approximately half the nominal drill spacing. For the neighbourhood dimensions, a first search pass for all deposits was set at between 40m by 30m by 5m to 70m by 40m by 10m. The second and third search passes were 1.5 and 3 times the first search. All final blocks were filled by a universal or infinite search. The search ellipse was oriented in accordance with the fitted variogram models: *Dip Direction: 75^{o}* *Dip: 35^{o}* *Plunge: 17^{o} (to the north-northeast)* For Jinkas footwall-White Dam a steeper plunge was used to capture high-grade gold shoots: *Plunge: 32.9°* As a result of the UC process, grade-tonnage curves of 2.5 by 2.5 by 2.5m Selective Mining Units (SMUs) are obtained for each panel. Using a technique called Localised Uniform Conditioning (LUC), individual SMUs are then estimated within each panel. Gold is deemed to be the only constituent of economic importance, and no by-products are expected. The model does not contain estimates of any deleterious elements. Gold mineralisation is associated with sulphides, with the dominant minerals being pyrrhotite, pyrite, chalcopyrite, and molybdenite. A previous estimation study for selected deposits in the KGP area was completed in December 2021. This study used different estimation techniques and parameters, and included a hybrid indicator method for Jinkas Footwall and White Dam Hanging-wall.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	The resource estimates are expressed on a dry tonnage basis, and in situ moisture content has not been estimated. A description of density data is presented below.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	A cut-off grade of 0.6 g/t Au has been used for resource reporting. An assessment of the geological data shows the mineralised lodes to be well defined at grade thresholds of 0.3 - 0.7 g/t Au. However, grades down to as low as 0.1 g/t Au also appear to define the continuity and were used occasionally in order to maintain continuous stationary domains. Ausgold has conducted preliminary financial modelling that indicates the use of a breakeven grade of less than 0.4 g/t Au based on assumed mining and processing costs and recoveries.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining*	Detailed mining studies have not yet been completed. It is expected that ore will be extracted using conventional selective open pit mining methods, which includes drilling and blasting, hydraulic

Criteria	JORC Code explanation	Commentary
	dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	excavator mining, and dump truck haulage. Mining dilution assumptions have not been factored into the resource estimates.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Detailed metallurgical test work is planned to be completed as part of a prefeasibility study. Preliminary metallurgical studies were performed in the 1980s and 1990s. Commentary in the study reports indicated recoveries exceeding 90% with modest reagent consumption, and that the gold was not refractory. In 2013 - 2014, oxide and sulphide ore bulk samples tested by Gekko Systems indicated that the material was amenable to gravity and cyanide leach processing, with expected recoveries exceeding 90%. In 2022 as part of Prefeasibility Studies Ausgold completed a comprehensive metallurgical test work program on five composites from 13 diamond drill holes in the Central and Southern Zones. Initial results were received from ALS Metallurgy under the supervision of an independent metallurgical consultant. Leach tests were completed on five composites. Three of these composites are from the Central Zone (Jinkas and Jinkas South lodes) and the Southern Zone (Dingo deposit). Recoveries from these samples indicate a consistently high gravity component from all samples with recoveries ranging between 40% up to 69% of total gold recovered. Leach test work indicates between 88-94% recoveries based on a 75 micron grind and 24 hour CIL residence time, with a low residue (tail) grade of 0.15g/t gold across the project. At a 53 micron grind and 48 hour residence, overall average gold recovery increases to 91-96%. Reagent usage was relatively low with less than 0.7 kg of cyanide (NaCN) consumed per tonne of ore on the Central Zones and less than 1kg/t on Southern Zones. Further studies will be undertaken as part of the definitive feasibility study.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early*	It is anticipated that material included in the resource will be mined under the relevant environmental permitting, which will be defined as a part of the feasibility studies. Work to characterise acid generating potential of waste material is underway and will be completed during a definitive feasibility study and factored into waste rock storage design. The future mine-cutback is in pastoral areas, with proximal homesteads, and Ausgold will continue to engage and inform landowners on matters such as noise, dust, vibration, discharge of surplus water, rainfall runoff, management of traffic movement and community consultation.

Criteria	JORC Code explanation	Commentary
	consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	Community consultation, including site visits by local Aboriginal elders, is also ongoing as part of the evolving exploration, mine planning and mine closure planning efforts.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	**In-Situ Samples** The KGP density dataset contains a total of 1,111 results, comprising 789 in-house water immersion tests performed on sealed core samples, 59 external water immersion tests conducted by ALS Metallurgy, 76 water replacement tests performed on pit samples, and 187 gamma logging tests conducted on RC holes. The in-house water immersion test core samples were acquired from 18 JINKAS holes, 2 WHITE DAM holes, 3 JACKSON holes, 2 OLYMPIA holes and 6 DINGO holes. The external ALS Metallurgy water immersion test samples were acquired from metallurgical composites from transitional to fresh JINKAS and transitional to fresh DINGO drill core. The gamma logging was performed on 7 JINKAS RC holes, and 39 and 37 pit samples were acquired from JINKAS and DINGO respectively. The samples were grouped according to weathering, with approximately 70% of the samples representing fresh material. The dataset averages were used to define a suitable density for each weathering type. For dry tonnage estimation, model cells were assigned the following dry *in situ* bulk densities based on weathering code and mineralisation (ore).: Oxide ore/waste = 1.8 t/m^3, Transition ore = 2.74 t/m^3, Transition waste = 2.71 t/m^3, Fresh ore = 3.1 t/m^3, Fresh waste = 2.81 t/m^3 **Tailings Material** The KGP density dataset contains a total of 9 samples for the tailings material. The density was calculated on dry samples through dividing the mass of the samples via the volume of the samples. The 9 samples were collected systematically over the tailings dam to include both fine and coarser tails material. The samples were collected in a container with a known volume of 2L (0.002M^3). An average of the density values of the 9 samples was calculated, which equated to 1.35 t/m^3.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of*	The resource classifications have been applied based on a consideration of the confidence in the geological interpretation, the quality and quantity of the input data, the confidence in the estimation technique, and the likely economic viability of the material.

Criteria	JORC Code explanation	Commentary
	input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The defined lodes can be traced over several drill lines and, although there is some evidence of localised pinching and swelling, they are generally quite consistent in terms of thickness, orientation, and grade tenor. It is considered that adequate QA/QC data are available to demonstrate that the Ausgold datasets, and by extension the historical datasets, are sufficiently reliable for the assigned classification. The model validation checks show a good match between the input data and estimated grades, indicating that the estimation procedures have performed as intended, and the confidence in the estimates is consistent with the classifications that have been applied. Past mining activities in the KGP area, and the numerous operations with similar mineralisation style and grade tenor within the Yilgarn Craton, support the potential economic viability of the deposits. Based on the findings summarised above, it was concluded that the controlling factor for classification was sample coverage. A resource boundary was defined approximately 15 m beyond the extents of relatively uniform drill coverage. An initial classification of Inferred was assigned to all blocks within the lodes. This was upgraded to Indicated in areas with a regular coverage of 30 x 30 m and/or where cells had been estimated by the second search pass and where there was high confidence in the continuity of the modelled lodes. A number of blocks were further upgraded to Measured where the regular coverage was 10 x 20 m, where most of the cells were estimated using the first search pass, and confidence in the continuity of the lodes was high.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	Snowden Optiro conducted an independent review of the Katanning Gold Project Mineral Resource in December 2021 and in May 2022.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	The resource estimates have been prepared and classified in accordance with the guidelines that accompany The JORC Code (2012), and no attempts have been made to further quantify the uncertainty in the estimates. The largest source of uncertainty is related to lode interpretation. However, based on pit exposures and core logging, general lode geometry is considered to be well understood and, coupled with the relatively dense data coverage, the likelihood of an alternative interpretation that would yield significantly different grade and tonnage estimates is considered to be low. In a stacked lode system, the incorrect linking of individual lodes between drill lines is possible, but the relatively close drill spacing would mean that any such occurrences may impact only upon the localised estimates and are not expected to significantly affect the regional or global estimates. The resource quantities should be considered as global estimates only. The accompanying models are considered suitable to support mine planning studies, but are not considered suitable for production planning, or studies that place significant reliance upon the local estimates.

Section 4 Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve* • *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	The Mineral Resource estimate for the KGP as at 25 May 2022 and as detailed in ASX release dated 25 May 2022 have been used for Ore Reserve estimation for the Katanning Gold Project. The Mineral Resource has been reported in accordance with the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC 2012). The 2020 Mineral Resource Estimate for the Katanning Gold Project is reported inclusive of the 2020 Ore Reserves
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	The 2020 KGP Ore Reserve Estimate was completed by Mr. Andrew Hutson FAusIMM. Mr. Hutson is employed by Resolve Mining Solutions. Mr. Hutson has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the mining activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC Code. Mr. Hutson has conducted a site visit to the Katanning project area. Discussions held have been factored into possible slope stability, ramp locations and networks, mining strategy, equipment selection, mine layout, waste dumping and other issues relative to the estimation of Ore Reserves.
Study Status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* • *The Code requires that a study to at least Pre- Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.*	The Katanning Mineral Resource has been converted to an Ore Reserve through the completion of a Prefeasibility Level Mining Study (PFS). The mine plan is considered technically achievable and involves the application of conventional technology and open pit mining methods widely utilised in the Western Australian goldfields. Financial modelling shows the project to be economically viable using current assumptions on gold price and quoted pricing. Material Modifying Factors that relate to mining and processing of ore and recovery of gold have been considered for the Ore Reserve Estimate.
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied*	Break-even cut-off grades were determined by considering: • Gold price; • Achievable gold recovery from ore processing (supported by metallurgical testwork);

Criteria	JORC Code explanation	Commentary
		• Mining costs, comprised of budget pricing obtained from the open pit mining contractors which were authenticated by a first principles cost estimate • Pre-Feasibility Study ore processing costs; and • Royalties
Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).* • *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.* • *The assumptions made regarding geotechnical parameters (e.g., pit slopes, stope sizes, etc), grade control and pre-production drilling.* • *The major assumptions made, and Mineral Resource model used for pit and stope optimisation (if appropriate).* • *The mining dilution factors used.* • *The mining recovery factors used.* • *Any minimum mining widths used.* • *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.* • *The infrastructure requirements of the selected mining methods.*	Conversion from Mineral Resource to an Ore Reserve was completed by detailed mine design. The first stage of open pit mine design involved automated modelling to generate conceptual "nested" pit shells. Pit shells were selected based on cashflow, geotechnical constraints and operational considerations. Detailed mine design was then carried out using the selected pit shell and wall design parameters provided by an external geotechnical consultant. Katanning is proposed to be mined via mechanised open pit methods utilising conventional mining equipment. The mining method has been selected based on orebody characteristics. The same mining method is currently being used to mine the nearby Jupiter Deposit. Independent geotechnical analysis reconfirmed this mining method and formed the basis of pit wall design criteria. A geotechnical assessment was completed by an external geotechnical consultant. Recommendations have been used during detailed mine design The Mineral Resource Model was used during the pit optimisation process. During pit optimisation, physical, technical and economic parameters were applied to the Mineral Resource Model generating "ideal" open pit excavation geometry which was carried through to detailed mine design. Ore loss (mining recovery) and dilution was modelled during the creation of the Resource Model and estimated taking into account ore width, orebody dip, the selective mining unit and the grade of the diluent material. Minimum mining bench widths of 30m were assumed based on selected mining equipment. No Inferred Mineral Resources have been included in the Ore Reserve Estimate. Inferred Mineral Resources were treated as waste and assigned no economic value.

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Metallurgical factors or assumptions	• *The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* • *Whether the metallurgical process is well-tested technology or novel in nature.* • *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* • *Any assumptions or allowances made for deleterious elements.* • *The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.* • *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	The proposed process flowsheet includes a Semi Autogenous Grinding, Ball Milling and Pebble Crushing (SABC) comminution circuit followed by conventional gravity and carbon-in-leach (CIL) process. The metallurgical process proposed is commonly used in Western Australian and international gold mining. An average metallurgical gold recovery of 91% was applied based on metallurgical testwork completed for the PFS in 2022. Testing was completed on the five main composites to optimise the recoveries and reagent additions. Optimised recovery and reagent consumption conditions were replicated for the variability samples to determine orebody variability, and confirm the oxide zone recovery and reagent consumptions (as the oxide will contribute to the ore blend). The testwork included resource area material considered for the PFS mill feed, providing a basis for engineering parameters to design the proposed processing plant, and economic evaluation. Not applicable. No minerals are defined by a specification.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation.* • *Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	The following environmental assessments have been undertaken across the Katanning Project mining tenure: • Biological studies –a number of flora/vegetation and fauna surveys have been undertaken and will continue seasonally to build a baseline data-set • Heritage studies – Aboriginal heritage surveys are complete. A Section 18 is granted and removal of artifacts has been completed by relevant knowledge holders • Waste characterisation – In progress, RC and diamond samples have been collected and samples that represent waste by lithology and weathering have been collected, acid-base accounting studies are in progress • Hydrological & Hydrogeological – monitoring bores have been established and a monitoring program commenced. Surface drainage management plans and dewatering assessments are in progress

Criteria	JORC Code explanation	Commentary
		The company is of the reasonable opinion that impacts associated with mine development at Katanning can be mitigated and minimised through the implementation of appropriate management measures and these are likely to be acceptable to regulators with respect to obtaining requisite project approvals.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	The Project site is located approximately 37 km from Katanning town, and is accessed through sealed and unsealed, public roads. The PFS assumes that the workforce will be accommodated in Katanning and identified housing and hotel opportunities appropriate for Project Execution and Operations. Other local opportunities identified include light-vehicle workshops and administration office. The PFS examined both dedicated power supply and connection to the existing grid, both of which are technically viable and fall within the economic parameters for unit cost for power supply. Other infrastructure will include a ROM pad, pit dewatering infrastructure, water supply bore field, mine services area (including offices, workshop, and stores), magazine, process plant offices and stores, wastewater treatment facility, tailings storage facility, and site roads.
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.* • *The methodology used to estimate operating costs.* • *Allowances made for the content of deleterious elements.* • *The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.* • *The source of exchange rates used in the study.* • *Derivation of transportation charges.* • *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.*	Capital costs are based on market rates as at the first quarter of CY2022 and are considered to be estimated at a +/-25% accuracy consistent with a PFS. Mining costs, comprised of budget pricing obtained from the open pit mining contractors which were authenticated by a first principles cost estimate. Mine owner operating costs have been estimated based on current site costs. All operating costs are considered to be estimated at a +/-25% accuracy consistent with a PFS. The average gold extractions for each material type (i.e., oxide, transitional, fresh) have been allowed for. Break-even financial analysis has been performed at a gold price of AUD$2200 per ounce. All revenue and cost calculations have been done using Australian Dollars; hence, application of an exchange rate has not been required.

Criteria	JORC Code explanation	Commentary
	• *The allowances made for royalties payable, both Government and private.*	Transportation and refining charges are based on budget quotations received from service providers. An allowance has been made for the 2.5% WA State Royalty. There are no private royalties payable.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* • *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	Ore production and gold recovery estimates for revenue calculations were based on detailed mine designs, mine schedules, mining factors and cost estimates for mining and processing. A gold price of $AUD2200 per ounce has been used for economic analysis.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* • *A customer and competitor analysis along with the identification of likely market windows for the product.* • *Price and volume forecasts and the basis for these forecasts.* • *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	There is a transparent quoted market for the sale of gold. No industrial minerals have been considered.
Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.*	The 2020 Katanning Ore Reserve Estimate has been evaluated through a standard financial model. All operating and capital costs as well as revenue factors were included in the financial model. This process has demonstrated the Ore Reserve Estimate has a positive economic return.

Criteria	JORC Code explanation	Commentary
	• *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	Sensitivity analysis has been carried out with significant assumptions and inputs varied by +/- 25%, which is consistent with the order of accuracy of PFS level assumptions and inputs. The Ore Reserve Estimate is most sensitive to mined grade, gold recovery and gold price.
Social	• *The status of agreements with key stakeholders and matters leading to social license to operate.*	Katanning Project is an historic mine site and has good working relationships with neighbouring stakeholders. Granted Mining Leases cover the Katanning Project Ore Reserve area. There are no existing or pending Native Title claims over the Katanning site.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:* • *Any identified material naturally occurring risks.* • *The status of material legal agreements and marketing arrangements.* • *The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.*	There are no likely identified naturally occurring risks that may affect the Katanning Ore Reserve Estimate area. There are reasonable grounds to expect that all necessary Government approvals will be received within standard timeframes after lodgement of requisite applications.
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.* • *Whether the result appropriately reflects the Competent Person's view of the deposit.* • *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	The classification of the 2022 KGP Ore Reserve Estimate has been carried out and reported in accordance with the 2012 Edition of the JORC Code. The 2022 KGP Ore Reserve Estimate reflects the Competent Person's view of the deposit. The Probable Ore Reserve is based on that portion of Measured and Indicated Mineral Resource within the mine designs that may be economically extracted and includes allowance for dilution and ore loss.

Criteria	JORC Code explanation	Commentary
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	Peer review on the 2020 KGP Ore Reserve Estimate has been completed internally by Resolve Mining Solutions.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.* • *It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	It is noted that Ore Reserve Estimates are an estimation only and subject to numerous variables common to mining projects and/or operations. It is however, in the opinion of the Competent Person that at the time of reporting, economic extraction of the 2020 Katanning Project Ore Reserve estimate can be reasonably justified. The mine design, mine schedule and financial model on which the Ore Reserve Estimate is based have been completed to a Pre-Feasibility Study standard with a corresponding level of confidence. Assumed ore treatment recoveries are supported by metallurgical testwork. It is in the opinion of the Competent Person that cost assumptions and factors applied in the estimation of the Ore Reserve are reasonable. Relevant contractor costs are based on budget level pricing supplied by suitably qualified mining contractors. There is reasonable grounds to expect that all primary and secondary mining approvals will be received within the timeframes required for project development.